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New Modeling Capabilities of GenCade for Simulation of Shoreline Changes in Northern Atlantic Coast

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US Army Corps of Engineers





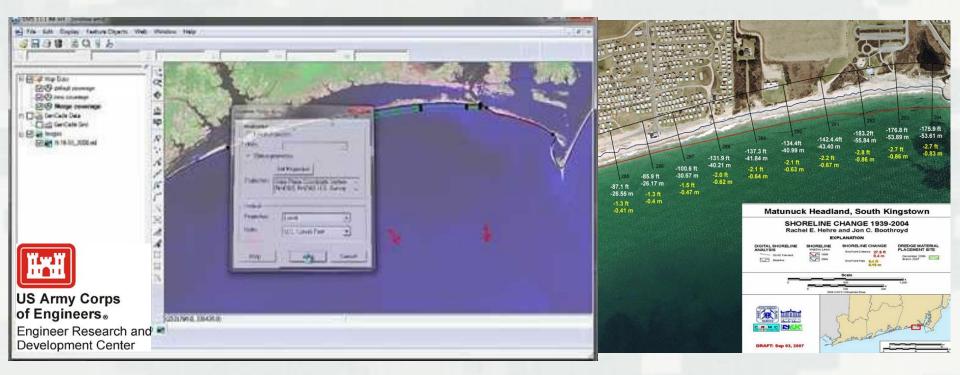
Outline

- Introduction of GenCade for Modeling Long-Term Shoreline Evolution
- New Features for Crossshore Sediment Transport and Sea Level Change
- Model Validation and Applications in Duck, NC
- Simulation of shoreline changes after beach fill in Delaware Coast (Ongoing Project)
- Remarks



GenCade

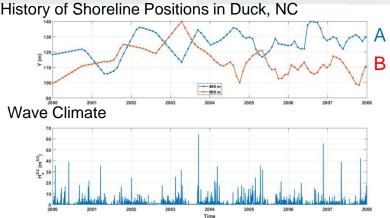
The GenCade (Frey et al. 2012) is a shoreline evolution model (a one-line model), using a alongshore sediment transport model to simulate shoreline changes driven by offshore wave climate. The SMS (Surfacewater Modeling System) provides a user-interface for GenCade, including data input and visualization



Long-Term Shoreline Changes

- Multiple physical processes drive shoreline changes: wave, wind, tide, storm, current, sea level change, sediment properties, longshore/crossshore sediment transport, human activities (structure installation, beach refill, beach recreation),etc.
- Shoreline changes induced by natural physical processes in general are highly irregular.
- Probabilistic shoreline change prediction is needed for best shoreline management practice for long-term protection purpose.
- Uncertainty estimation of shoreline changes is required for best shoreline erosion control management.





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GenCade Shoreline Evolution Model with Cross-Shore Transport and SLR

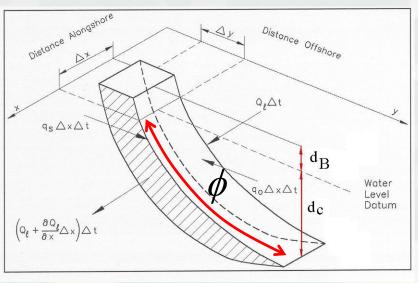
Shoreline Change Equation with Sea Level Rise (SLR)

$$\frac{\partial y}{\partial t} + \frac{1}{D_s} \left(\frac{\partial Q}{\partial x} - q - \phi \right) + \left(\left(\frac{\Delta Z}{\Delta t} \right)_{SLR} - \left(\frac{\Delta Z}{\Delta t} \right)_{subsidence} \right) \frac{1}{\tan \beta} = 0$$

: Cross-shore sediment transport rate

 $(\frac{\Delta Z}{\Delta t})_{SLR}$: Sea Level Change Rate $(\frac{\Delta Z}{\Delta t})_{subsidence}$: Sea Level Change Rate $tan\beta$: beach slope

- $D_{\rm S} = d_{\rm c} + d_{\rm b}(t)$
- Berm height varies with sea level change $d_b(t) = d_{b0} - \left(\left(\frac{\Delta Z}{\Delta t}\right)_{SLR} - \left(\frac{\Delta Z}{\Delta t}\right)_{subsidence}\right)t$



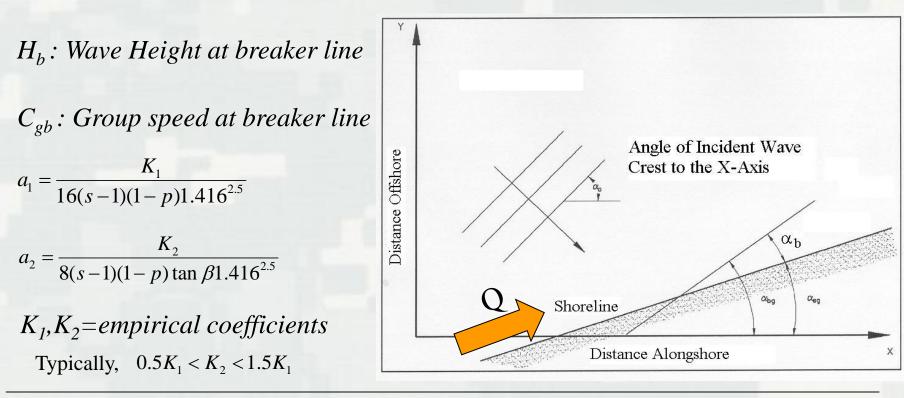
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Longshore Sediment Transport Energy Flux Method (CERC formula)

$$Q = H_b^2 C_{gb} \left(a_1 \sin 2\alpha_b - a_2 \cos \alpha_b \frac{\partial H_b}{\partial x} \right)$$



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New Feature of GenCade (1) - Cross-shore Sediment Transport due to Wave Asymmetry and Nonlinearity

Transport Rate due to Velocity Skewness (Hsu et al. 2006)

 $\phi = \frac{\alpha_D}{1-p} (Q_V + Q_C + Q_D) \qquad \qquad \alpha_D = \text{empirical parameters, } p = \text{porosity of sediment}$

 Q_v and Q_c are the net sediment transport due to waves and currents

$$Q_{V} = \frac{C_{W}}{(s-1)g} \left(\frac{\varepsilon_{B}}{\tan \varphi} < \left|\vec{U}_{0}\right|^{2} U_{0,x} > + \frac{\varepsilon_{S}}{W_{0}} < \left|\vec{U}_{0}\right|^{3} U_{0,x} > \right)$$
$$Q_{C} = \frac{C_{C}}{(s-1)g} \left(\frac{\varepsilon_{B}}{\tan \varphi} < \left|\vec{U}_{t}\right|^{2} U_{x} > + \frac{\varepsilon_{S}}{W_{0}} < \left|\vec{U}_{t}\right|^{3} U_{x} > \right)$$

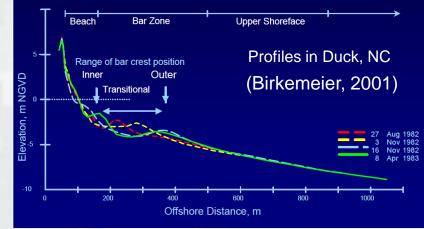
 U_0 = the wave orbital velocity vector, U_t = the total velocity vector (waves plus currents), and U = the current velocity vector, related to longshore current and undertow current.

 φ = the friction angle

 W_0 = the sediment fall velocity

 $Q_D = \frac{\lambda_d v \tan \beta}{\tan \varphi (\tan \varphi - \tan \beta)}$

 $C_{w}, C_{C}, \varepsilon_{B}, \varepsilon_{S}$ = empirical parameters



 Q_D represents a diffusive transport due to downslope move of sand:

 λ_D , v=empirical parameters

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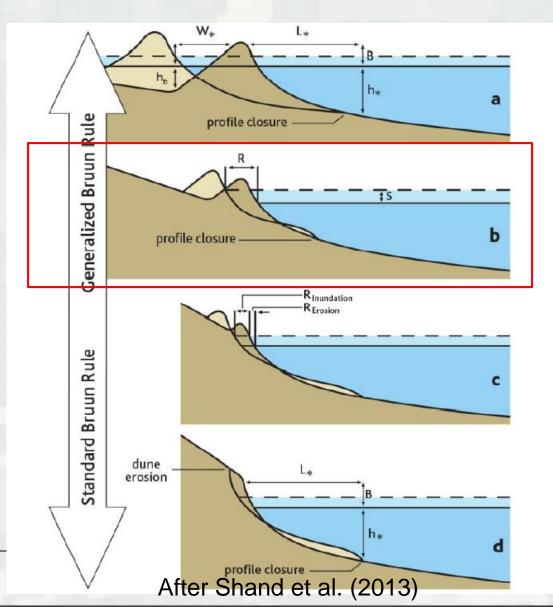
New Feature of GenCade (2) - Shoreline Recession due to Sea Level Rise:

Shoreline Retreat rate

Bruun Model (1962, 1988)

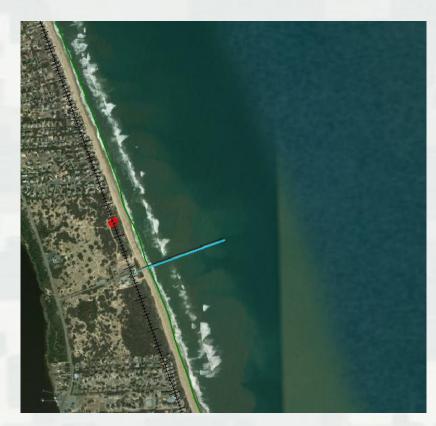
 $R = \frac{SW_*}{h_* + B}$

S: Sea level rise rate h* = sediment closure depth B = Berm Height



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Model Validation: Modeling of Shoreline Change in Duck, NC

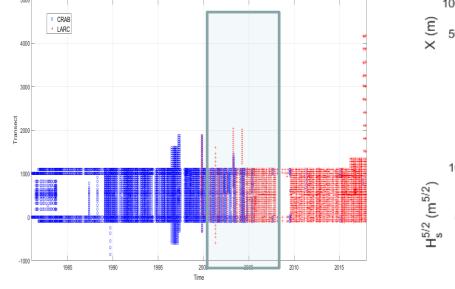


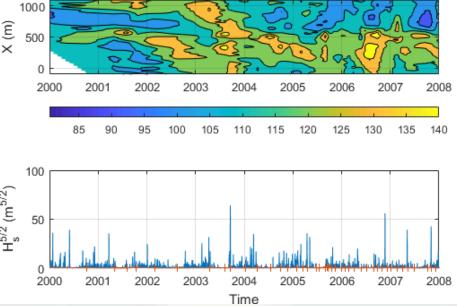
FRF in Duck, NC

Computational Period: 6 years 1999/10/23 0:00 - 2005/10/23 0:00 Time step = 3 minutes Grain size = 0.20 mm Berm Height = 1.0 m Closure depth = 7.0 Smooth parameter = 1 (no smoothing) Boundary Conditions: Pined Grid Size = 20 m Sea Level Rise rate: 4.55mm/year Subsidence : 0.0 (N/A)

Calibrated Model Parameters: K1 = 0.40 K2 = 0.25Permeability of Pier = 0.6 (no diffracting): Scaling parameter $\alpha_D = 0.182$ $C_w, C_C, \varepsilon_B, \varepsilon_S$ by Fernández-Mora et al. (2015)

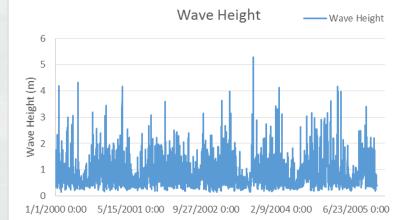
V&V of GenCade for FRF Shoreline: Data Analyses



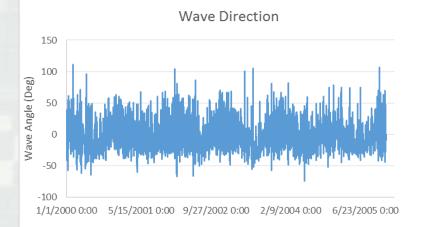


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Wave Data (2000/1/1 - 2006/1/1)

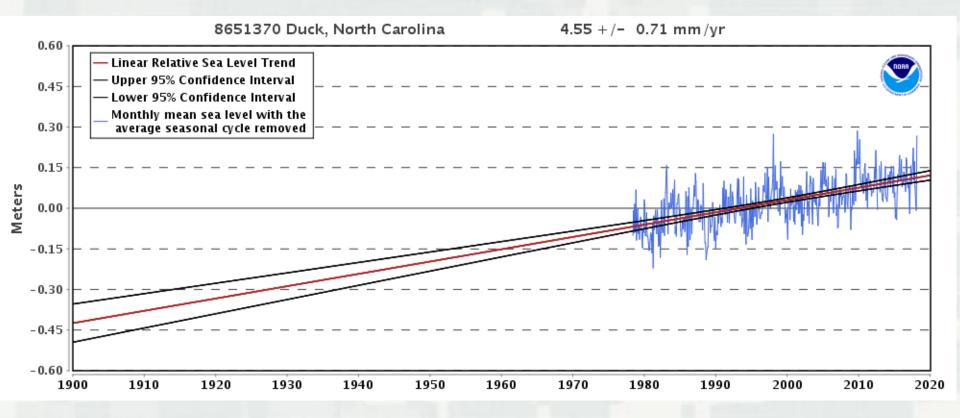


	H (m)	T (s)	alfa (deg)
Average	0.82	9.18	-5.06
Min	0.14	3.09	-74.62
Max	5.28	18.96	111.32
σ	0.53	2.68	18.52



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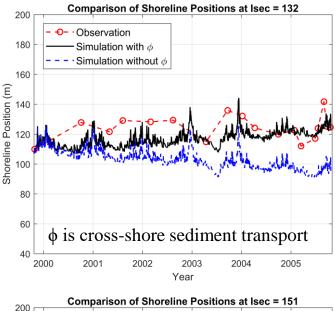
Sea Level Rise Trend NOAA-NOS #8651370 Duck, North Carolina

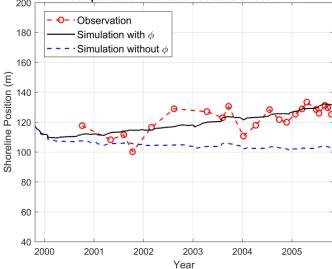


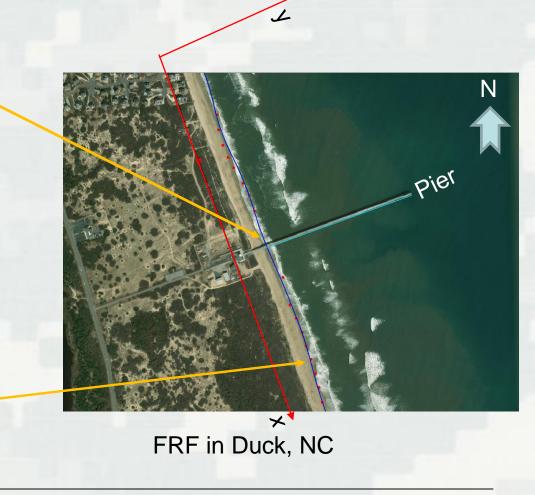
https://tidesandcurrents.noaa.gov/sltrends/sltrends_station.shtml?id=8651370

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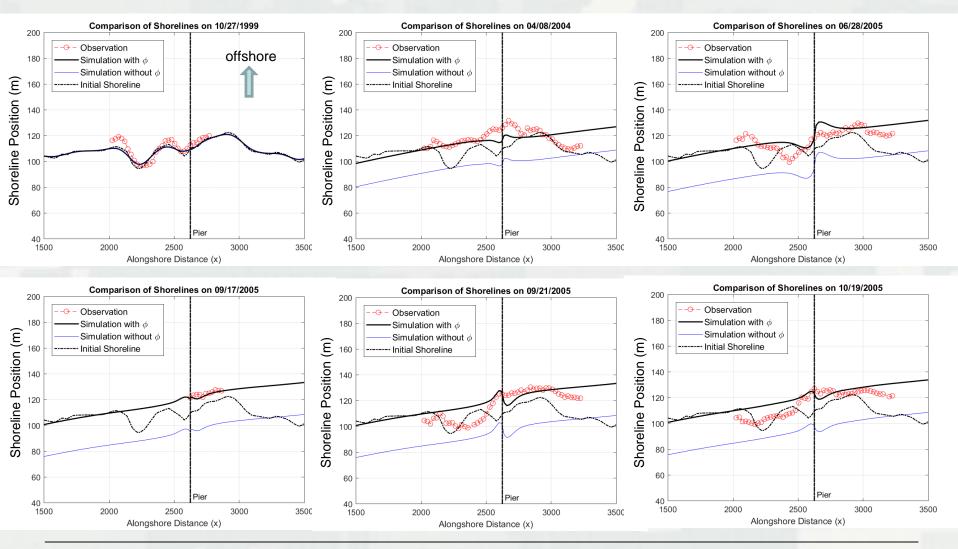
Model Validation: Comparison of Shoreline Evolution (1999-2005) at FRF, Duck, NC





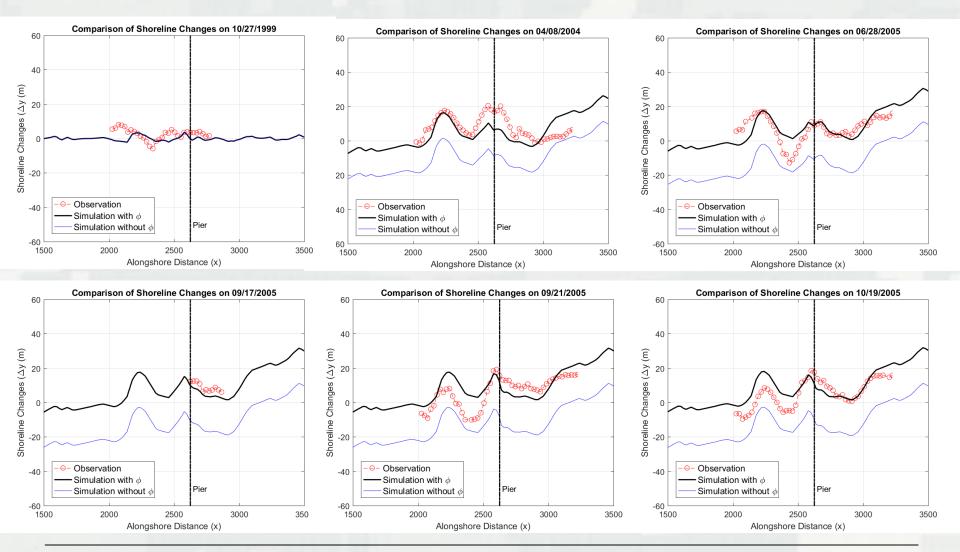


Model Validation: Comparisons of Shoreline Positions (1999-2005)



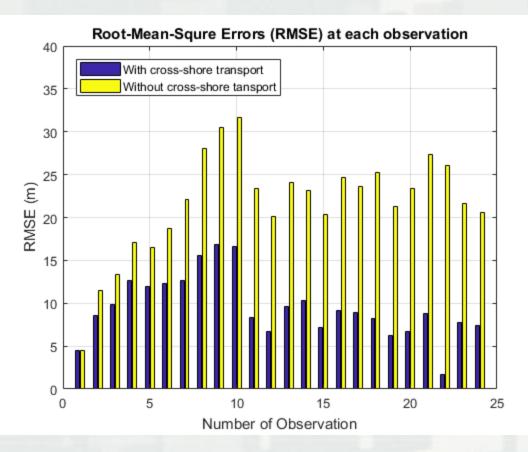
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Model Validation: (w or w/o xshore) Comparisons of Shoreline Changes (1999-2005)

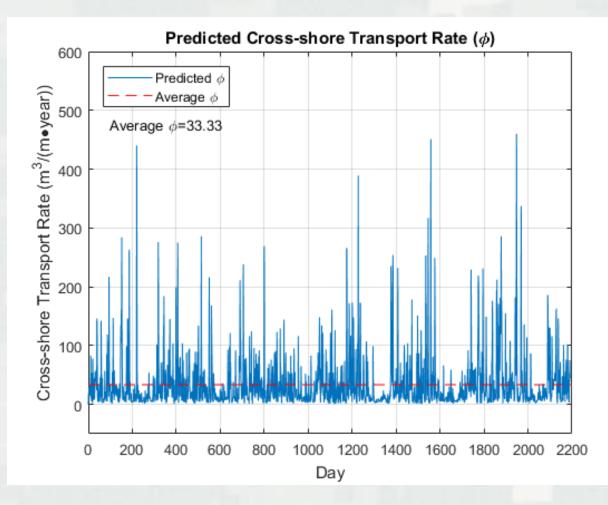


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Model Skill Assessment: Root-Mean-Square Errors at Observation Times (1999-2005)



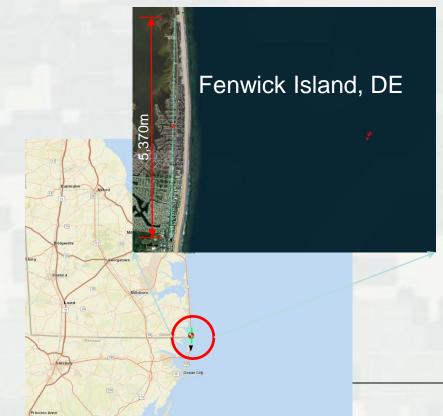
Predicted Cross-Shore Transport Rate (1999-2005)



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Modeling of Shoreline Change in Fenwick Island, DE

Objectives: (1) to validate the GenCade model by using shoreline survey data provided by NAP and DNREC, and (2) to evaluate shoreline erosion after beach fill completed in Sept. 2013.



Computational Parameters

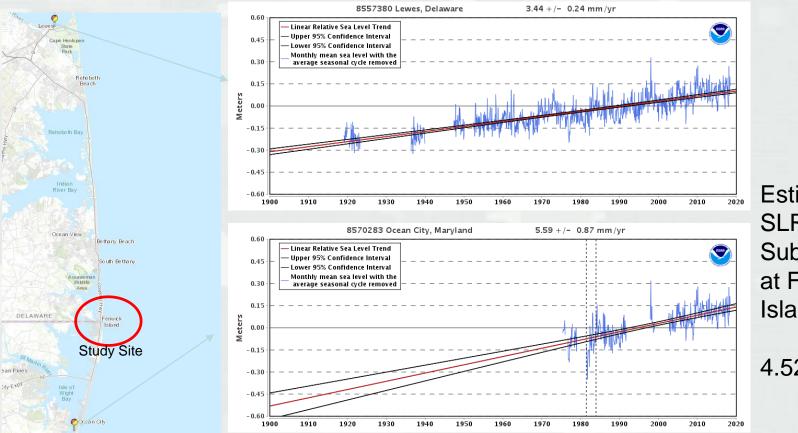
Computational Period: 3.5 years 2013/09/13 0:00 - 2017/01/01 0:00 after the beach fill in Sept. 2013

Time step = 3 minutes Grain size = 0.30 mm Berm Height = 1.0 m Closure depth = 10.0m Smooth parameter = 1 (no smoothing) No regional contour Boundary Conditions: Moving (retreat 2.5 ft/year) Grid Size = 20 m Sea Level Rise rate: 4.50mm/year (based on tide gauges) Subsidence : included

Calibrated Model Parameters: K1 = 0.90K2 = 0.35

Cross-shore transport included Scaling parameter $\alpha_D = 0.16$ $C_w, C_C, \varepsilon_B, \varepsilon_S$ by Fernández-Mora et al. (2015)

Relative Sea Level Rise in Delaware Coast

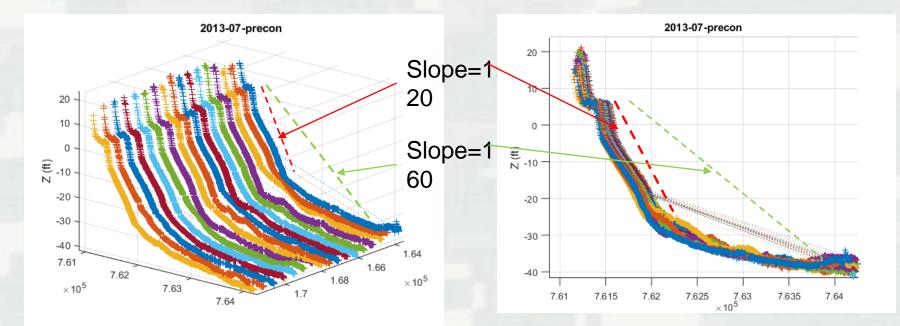


Estimated SLR and Subsidence at Fenwick Island

4.52mm/yr

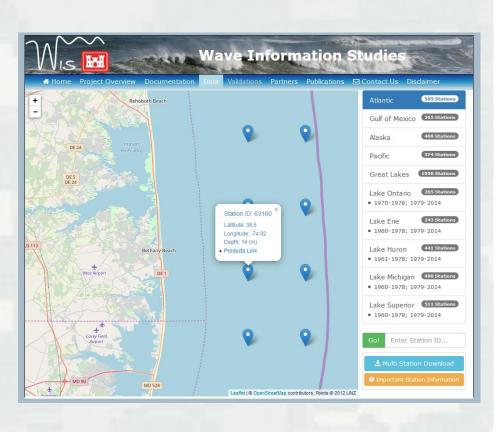
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Beach Slope

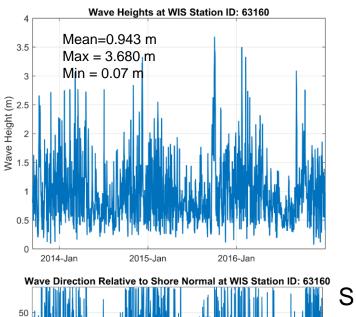


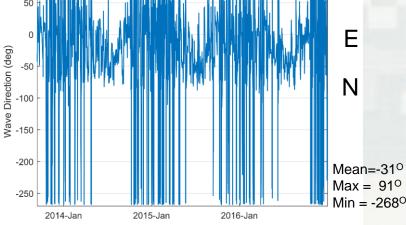
17 Survey Transects

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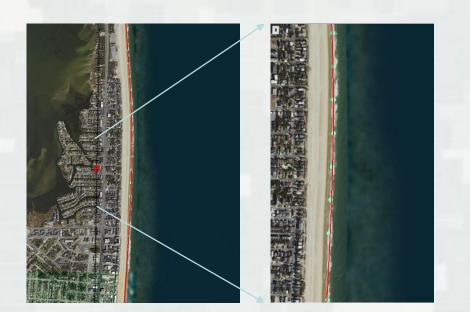
Waves





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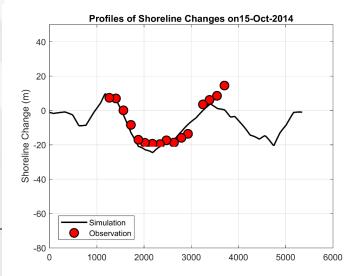
Comparisons of Shoreline Positions on 10/15/2014 (after one year)



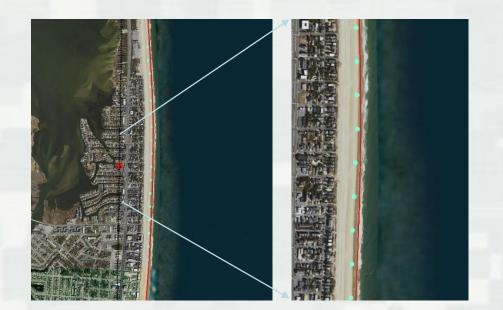
Shoreline Change from Sept. 2013-Oct. 2014: -20.0m \rightarrow + 10.0m

500 Initial Simulation 450 Observation 400 Position (m) 350 Shoreline 300 250 200 150 1000 2000 3000 4000 5000 6000 Ω

Profiles of Shoreline Positions on15-Oct-2014

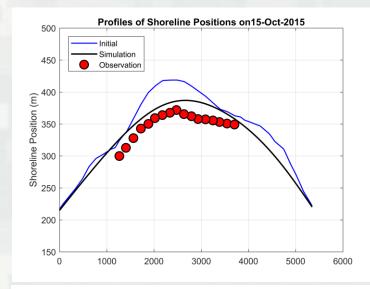


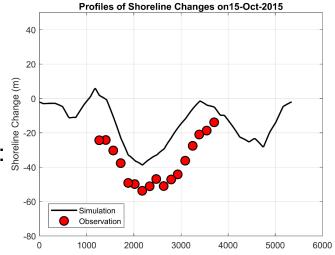
Comparisons of Shoreline Positions on 10/15/2015 (after two years)



2.5-year Shoreline Change from Sept. 2013-Oct. 2015: $-50.0m \rightarrow + 5.0m$

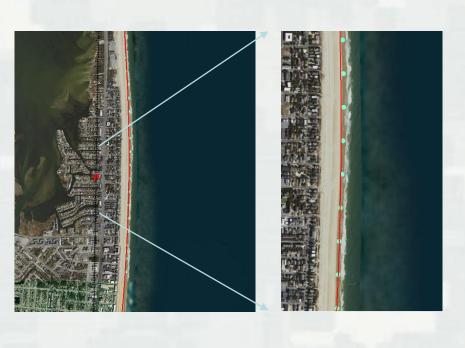
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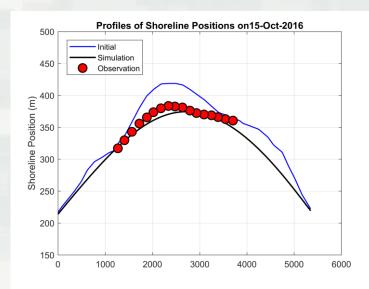


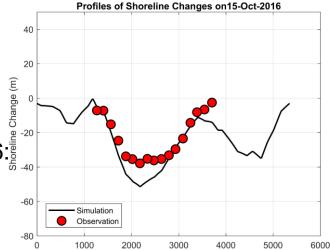


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Comparisons of Shoreline Positions on 10/15/2016 (after three years)



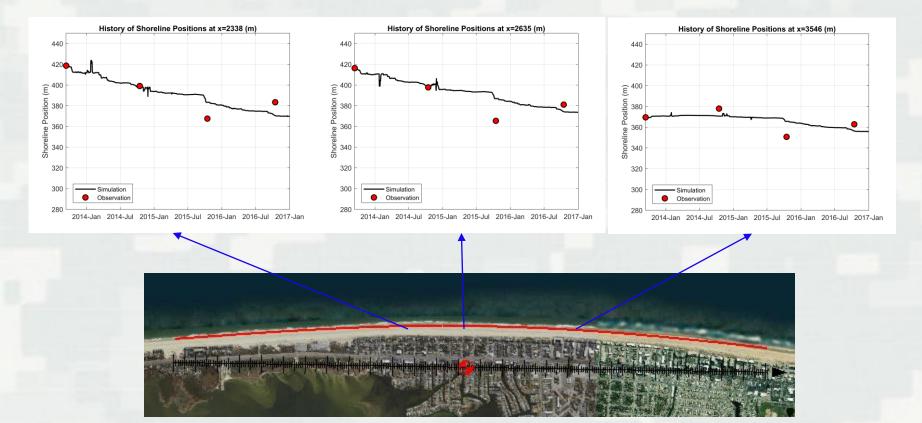




3.5-year Shoreline Change from Sept. 2013-Oct. 2016: $-50.0m \rightarrow + 0.0m$

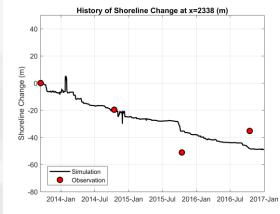
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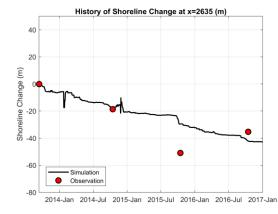
History of Shoreline Positions in Fenwick Island, DE

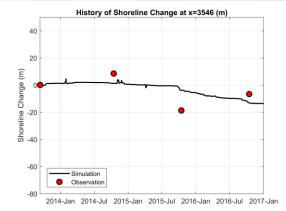


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History of Shoreline Changes in Fenwick Island, DE



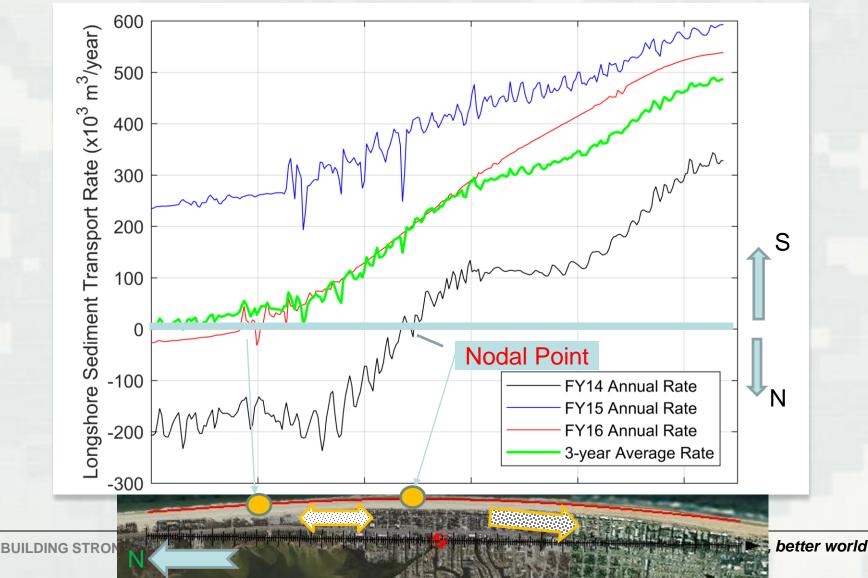




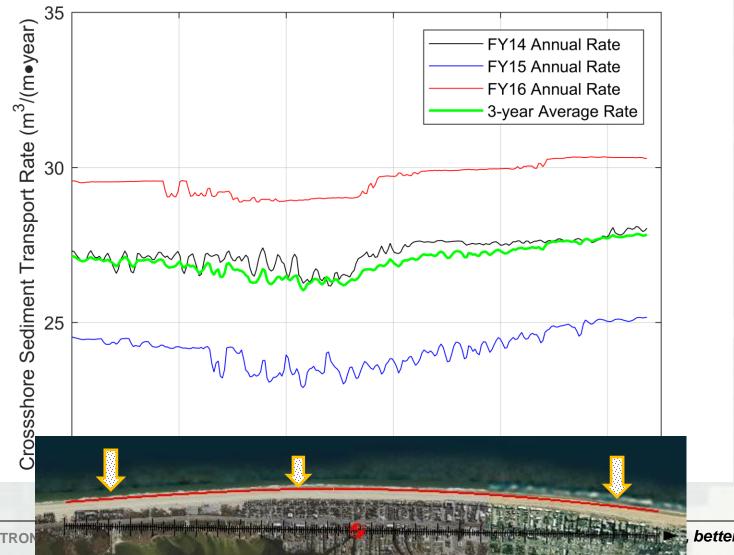


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Annual Longshore Sediment Transport Rate in Fenwick Island, DE



Annual Crossshore Sediment Transport Rate in Fenwick Island, DE



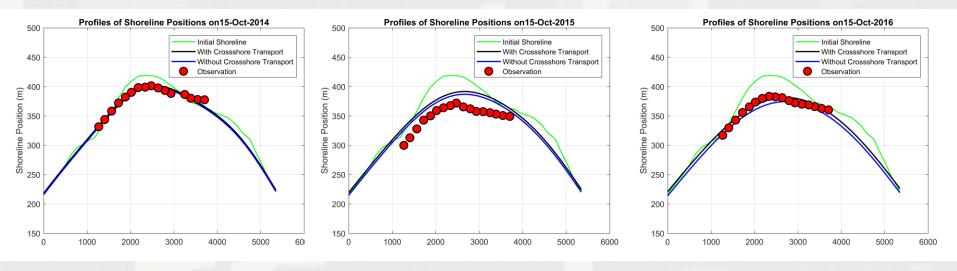
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History of Longshore and Crossshore Sediment Transport Rate



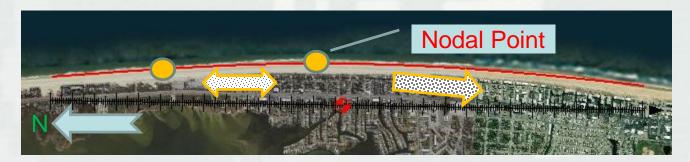
Comparisons of Shoreline Positions Computed with and without Crossshore Transport



(1) After one year (10/15/2014)

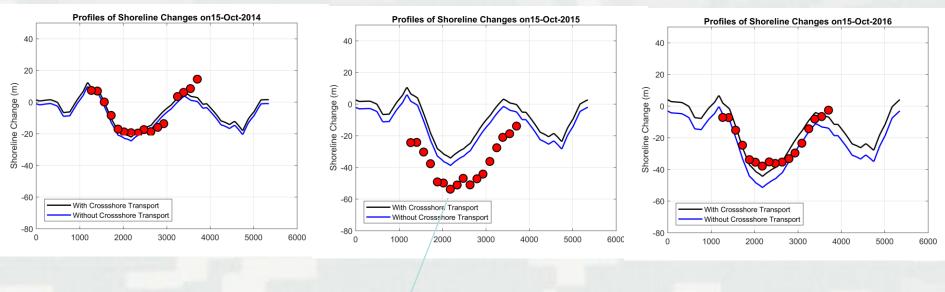
(1) After two years (10/15/2015)

(1) After Three year (10/15/2016)



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Comparisons of Shoreline Changes Computed with and without Crossshore Transport



(1) After one year (10/15/2014)

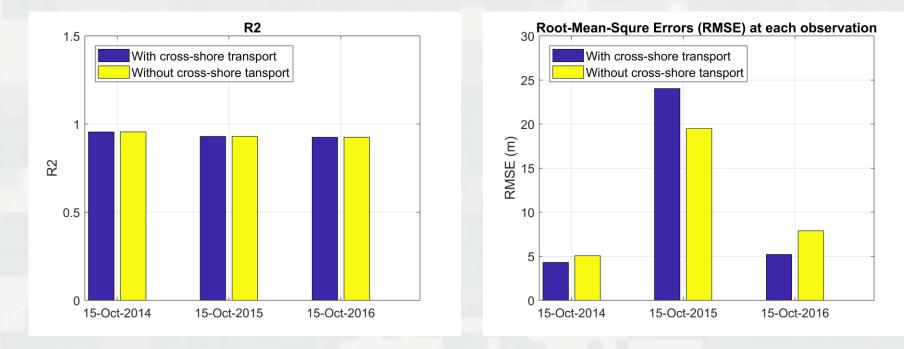
(1) After two years (10/15/2015)

(1) After Three year (10/15/2016)



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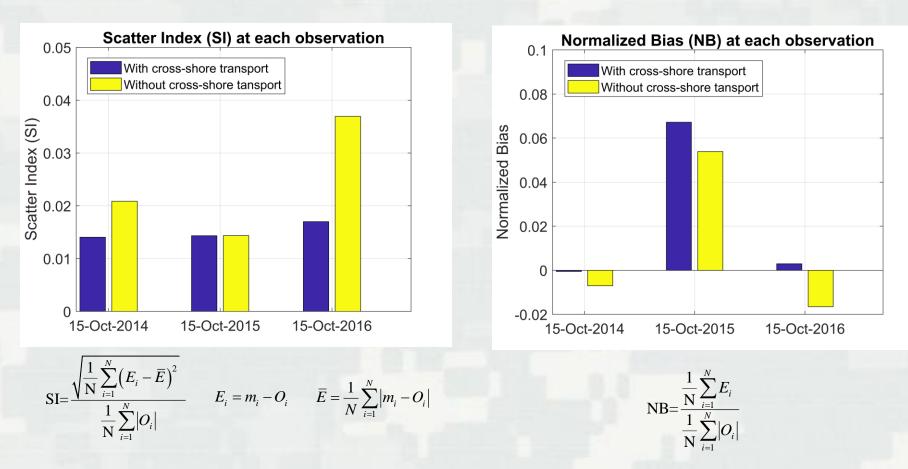
Model Skill Assessment Results (1)



Remarks:

- (1) R2 values close to unity \rightarrow GenCade simulation results are consistent with the real shoreline shores.
- (2) Adding crossshore sediment transport improved model results in 2014 and 2016.
- (3) Large RMSEs in Oct. 2015 need to be investigated.

Model Skill Assessment Results (2)



Remarks:

With cross-shore transport, the model reduces the scattered results and bias.

Remarks

- Newly-developed model capabilities of GenCade enhance model's applicability to predict shoreline evolution with a higher accuracy driven by multiple physical processes such as longshore and cross-shore sediment transport, shoreline retreat due to sea level rise, nearshore wave processes (nonlinearity, undertow, gravity, etc).
- Cross-shore sediment transport is an important process in simulating shoreline evolution in Duck, NC. Nonlinearity of waves plays an important role in driving net cross-shore transport in nearshore zone.
- Longshore sediment transport is a predominant process to erode the Fenwick Island shoreline, DE. But the crossshore sediment transport in the coast is also important to balance the beach erosion. By taking into account both long- and cross-shore processes GenCade can give a better assessment of beach filling in the DE coasts.
- GenCade with Monte-Carlo simulation provides a useful approach to assess uncertainty of shoreline change prediction. Preliminary results of probabilistic shoreline changes in Duck, NC are reasonable. Estimation of extreme shoreline changes provides risk of erosion in a return-interval manner.
- Sea level change is an important factor for predicting long-term shoreline changes (esp. erosion due to sea level rise).

Thank you!