Probabilistic Shoreline Change Simulation for Risk Estimation of Shoreline Erosion



Shoreline Change

& Protection

Structures (jetty, groin, breakwater,

Barrier Island Dredging Beach fill

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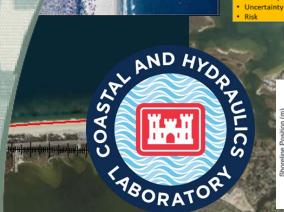
U.S. Army Engineer Research and Development Center (ERDC), Coastal and Hydraulics Laboratory (CHL)

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US Army Corps of Engineers_®







GenCade

GenCade-Based

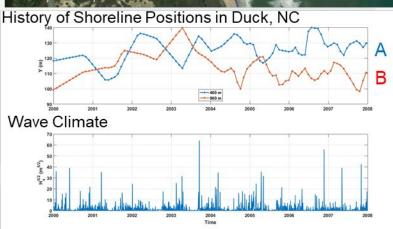
Outline

- ➤ Introduction: Motivation, Objectives, and GenCade
- GenCade-based Monte-Carlo Simulation for Risk Estimation of Shoreline Change
- Case Studies for Risk and Uncertainty of Long-Term Shoreline Changes
 - Idealized Coast
 - Duck coast at FRF, NC
 - Fenwick Island, DE (Uncertainty by Beach Fill)
- > Remarks

Risk and Uncertainty in Long-Term Shoreline Changes

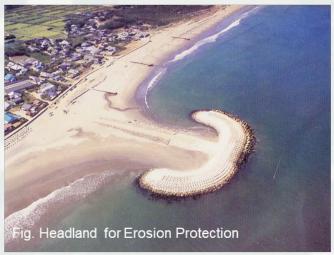
- Quantifying erosion risk and uncertainty in simulating long-term shoreline changes is an important task in risk-based coastal management practice.
- Multiple physical processes drive shoreline changes: wave, wind, tide, storm, current, sea level change/subsidence, sediment properties, longshore/cross-shore sediment transport, etc.
- Coastal development: structure installation, beach refill, beach recreation, etc.
- Shoreline changes induced by natural physical processes in general are highly irregular. And uncertainty in coastal protection practice exists
- Probabilistic shoreline change (Monte-Carlo) simulation is an effective way to quantify risk and uncertainty of shoreline changes driven by physical processes and coastal protection practices.





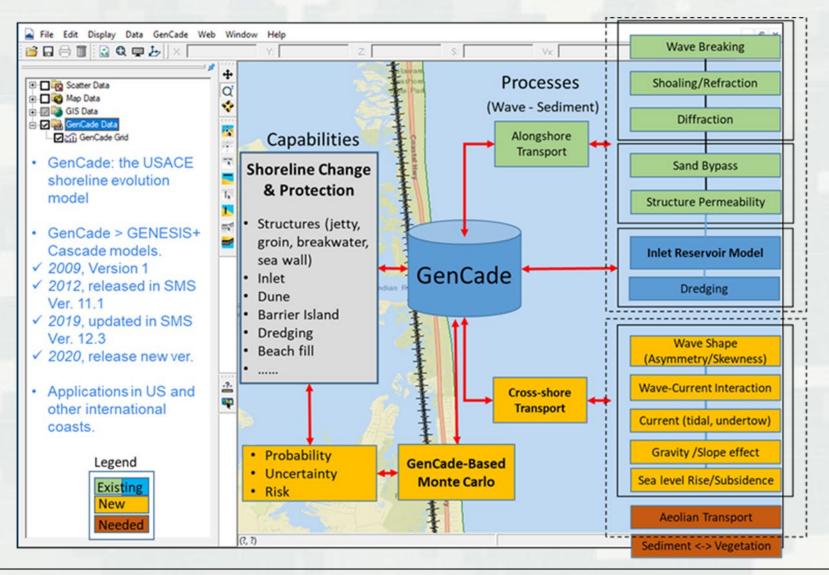
Uncertainties in Shoreline Changes due to Coastal Management Practices

- Construction or modification of inlets for navigational purpose
- Construction of harbors with breakwaters built in nearshore regions
- Beachfills (sand nourishment)
- Sand Bypass
- Sand Mining
- Dredging Material Disposals

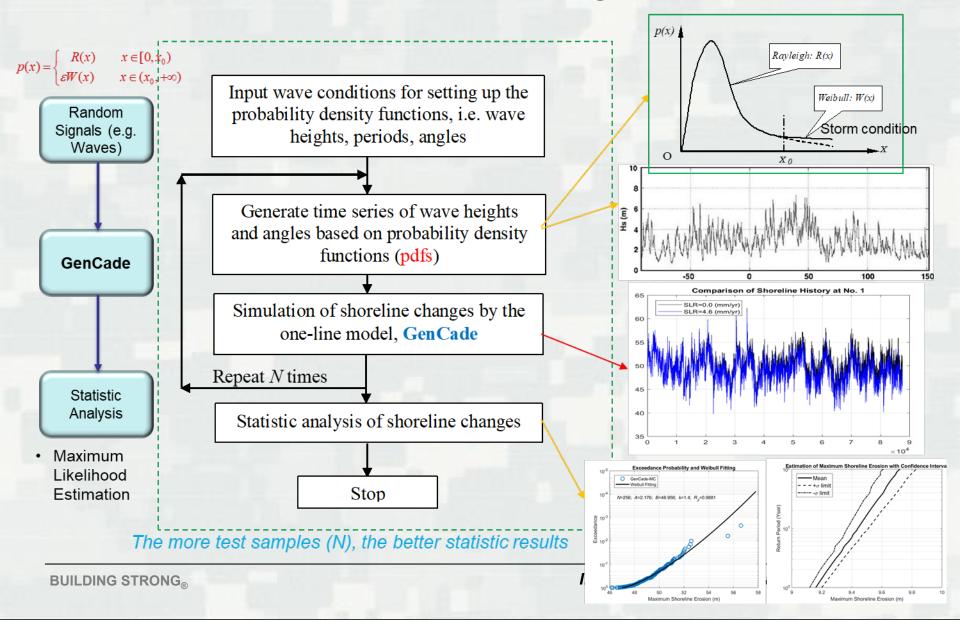




GenCade for Simulating Shoreline Evolution

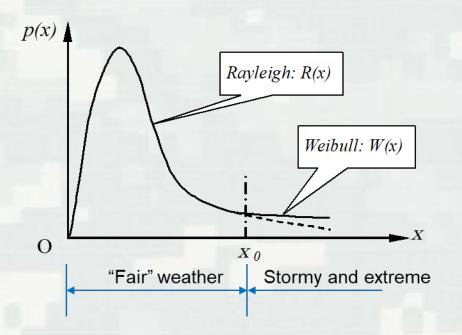


GenCade-Based Monte Carlo Simulation: Estimation of Uncertainty and Risk



Generate Random Wave Signals Using Probabilistic Density Function (PDF) of Wave Height

Consider waves in "fair" weather and storms: Non-Gaussian PDF with a fat-tail shape



$$\int_{-\infty}^{+\infty} p(x) = 1 \quad \Longrightarrow \varepsilon = \frac{e^{-\frac{\pi}{4}x_0^2}}{e^{-(\frac{x_0 - B}{A})^K}}$$

$$p(x : \varepsilon, R, W) = \begin{cases} R(x) & x \in [0, x_0) \\ \varepsilon W(x) & x \in (x_0, +\infty) \end{cases}$$

where $x = {}^{H}/_{\overline{H}}$, \overline{H} : mean wave height ε : parameter x_0 : a truncated extreme value of wave height

Rayleigh Distribution (for normal waves):

$$R(x) = -\frac{\pi}{2} x \exp\left(-\frac{\pi}{4} x^2\right) \qquad x \le x_0$$

Weibull Distribution ("fat-tail" for extreme waves):

$$W(x:k,A,B) = \frac{1}{k} \left(\frac{x-B}{A}\right)^{k-1} \exp\left(-\left(\frac{x-B}{A}\right)^k\right)$$
$$x > x_0$$

How to Determine the "fat-tail" PDF? Wave Observation Data: An Example

Density distribution of wave height is fitted as mixing distribution of Rayleigh and Weibull distributions

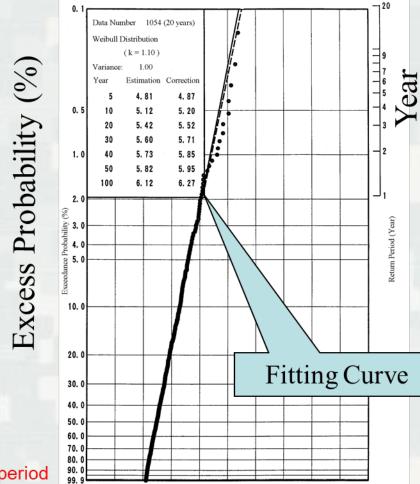
$$p(x) = \begin{cases} R(x) & x \in [0, x_0) \\ \varepsilon W(x) & x \in (x_0, +\infty) \end{cases}$$

where
$$x = H/H_{mean}$$
,
in $W(x)$, $k = 1.1$, $A = 0.5792$, $B = 2.0554$, $x_0 = 2.1$

$$\bar{H} = 1.19 \text{ m}$$

Observation data: H=4.0 m wave height for one-year return period

Observation data at Naka Port, Japan, from 1980 to 1996



Wave Height (m)

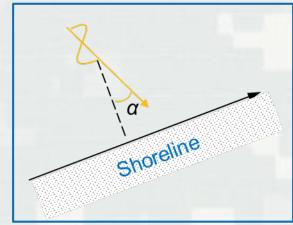
Wave Direction and Period

Incident Wave Angle (α): Gaussian Distribution

$$p(\alpha) = N(\alpha \mid \mu, \sigma) = \frac{1}{\sqrt{2\pi}\sigma} \exp\left(-\frac{(\alpha - \mu)^2}{2\sigma^2}\right) \qquad \alpha \in [-\frac{\pi}{2}, +\frac{\pi}{2}]$$

 σ : Standard deviation of wave direction

 μ : Mean value of direction



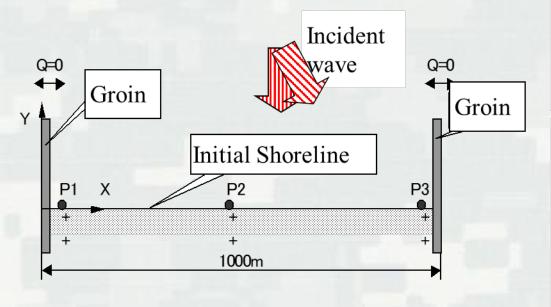
Significant Wave Period: based on Pierson-Moskowitz Spectrum

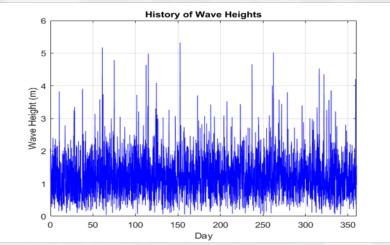
$$T_s = 5\sqrt{H_s}$$

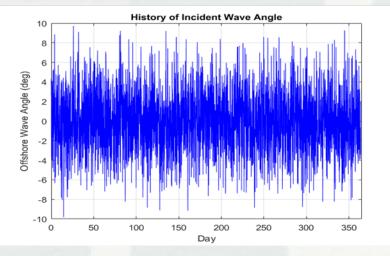
Probabilistic Shoreline Change Modeling in an Idealized Coast: Sensitivity Study

Two Test Cases:

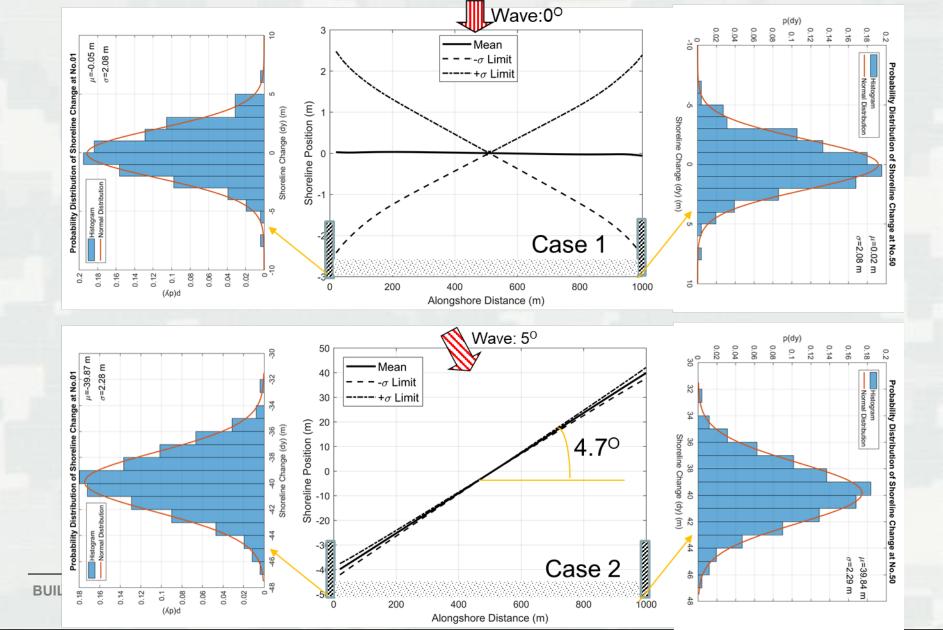
- (1) Case 1 ($\alpha_{\text{mean}} = 0.0^{\circ}$)
- (2) Case 2 ($\alpha_{mean} = 5.0^{\circ}$)



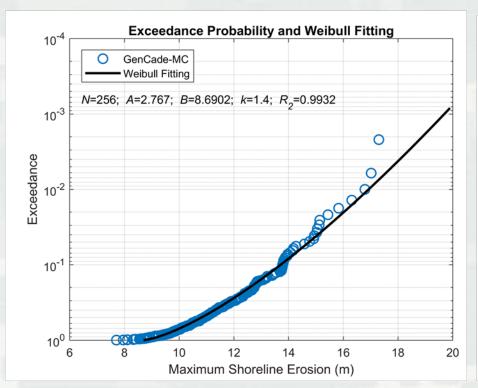


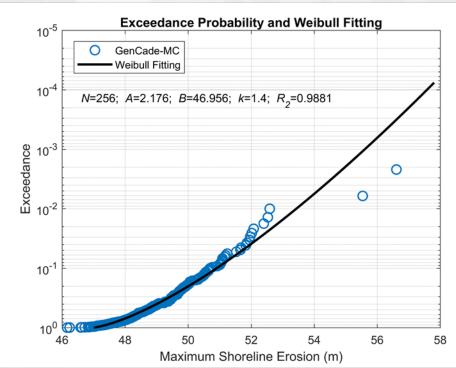


Predictions of Mean Shoreline Changes after 10 Years



Estimation of Maximum Shoreline Erosion (Landward most) in the Future: Maximum Likelihood Estimation





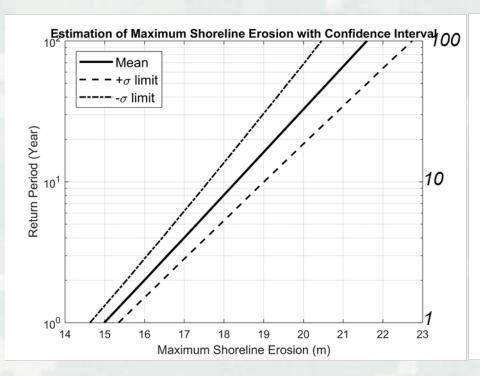
(1) Case 1 ($\alpha_{mean} = 0.0^{\circ}$)

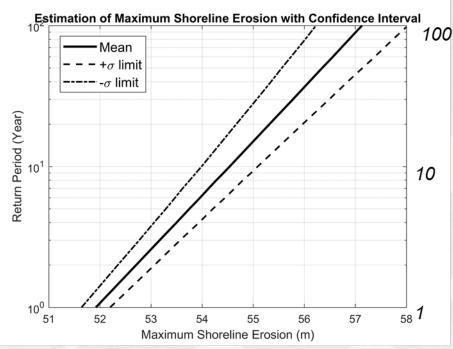
Weibull Function Best Fitting

$$F(\Delta y) = 1 - \exp\left[-\left(-\frac{\Delta y - B}{A}\right)^{k}\right]$$
 (k=0.75~2.0)

(2) Case 2 ($\alpha_{mean} = 5.0^{\circ}$)

Prediction of Maximum Shoreline Erosion (Landward most) near Groin - Maximum Erosion in the Future





(1) Case 1 ($\alpha_{\text{mean}} = 0.0^{\circ}$)

R = 1

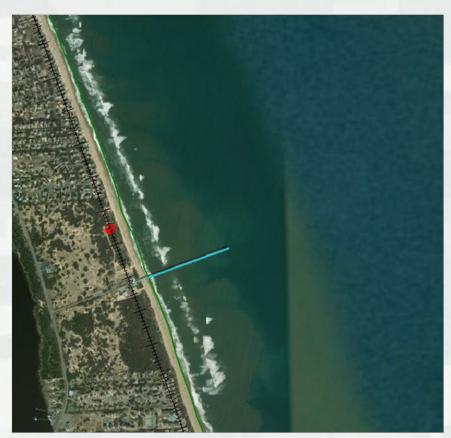
(2) Case 2 ($\alpha_{\text{mean}} = 5.0^{\circ}$)

Return Period (year): R

(λ: mean rate of date samples)

Goda, Y., (1988). On the methodology of selecting design wave height. In: B.L.Edge, Proc. of the 21st ICCE. ASCE, pp. 899–913.

Monte Carlo Simulation of Shoreline Change in Duck, NC



FRF in Duck, NC

Number of Monte Carlo = 128
Wave Conditions:

Wave Height: Rayleigh+Weibull

Direction: Gaussian Period: PM Spectrum

Truncated Wave Height: 2.0 m

Computational Period: 6 years

1999/10/23 0:00 - 2005/10/23 0:00

time step = 3 minutes

K1 = 0.40; K2 = 0.25

Grain size = 0.20 mm

Berm Height = 1.0 m

Closure depth = 7.0

Sea Level Rise Rate = 4.55 mm/year

Smooth parameter = 1 (no smoothing)

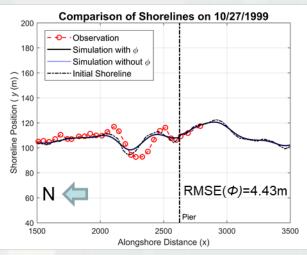
Boundary Conditions: Pined

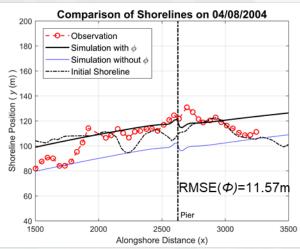
Grid Size = 20 m

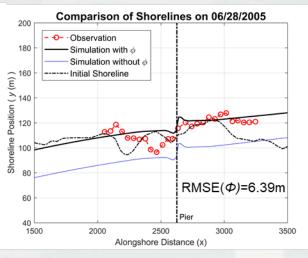
Permeability of Pier = 0.6 (no diffracting)

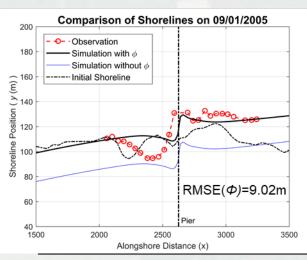
Scaling parameter of cross-shore transport: 0.182

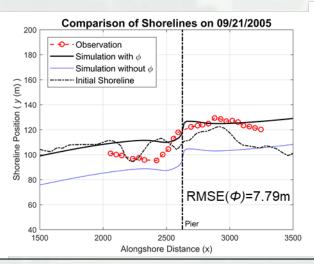
Model Validation -Determine System Errors

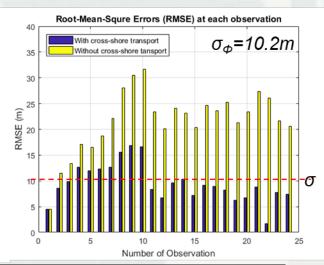




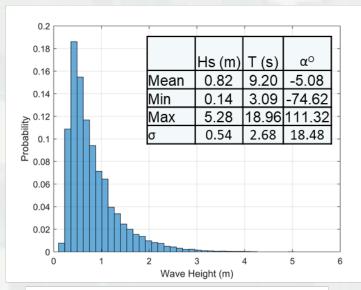


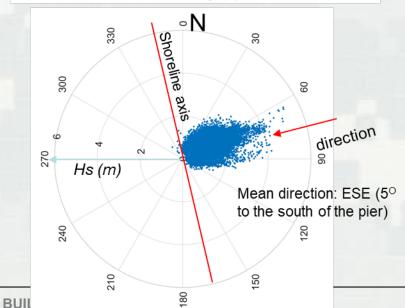


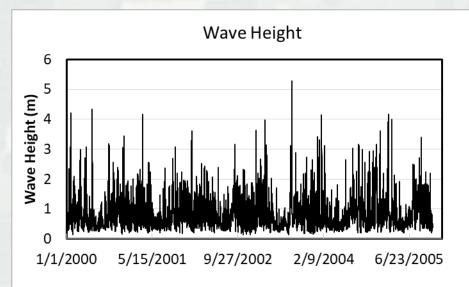


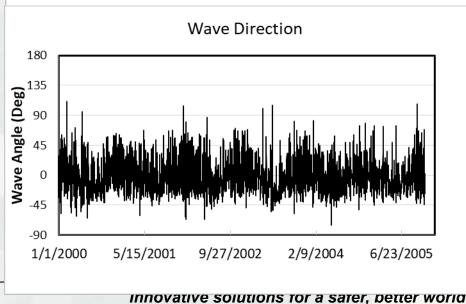


Wave Data for Creating PDFs



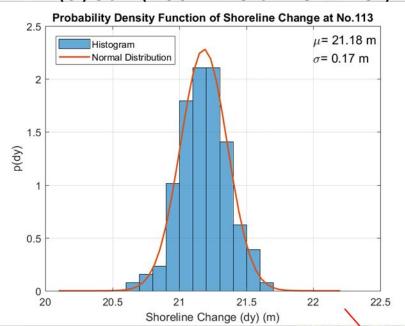




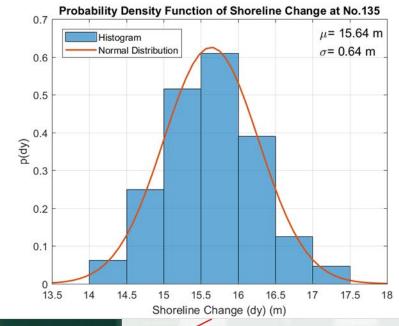


Probability Density Functions: 6-Years Shoreline Change

(a) at A (400-m north from Pier)

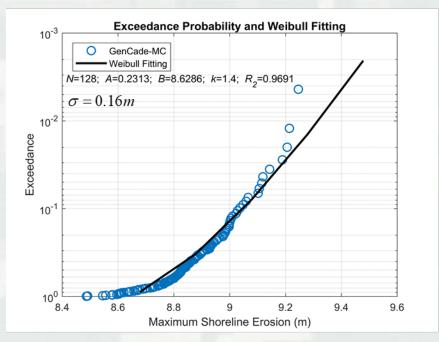


(b) at B (40-m south from Pier)

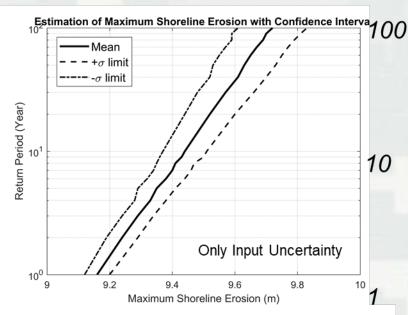


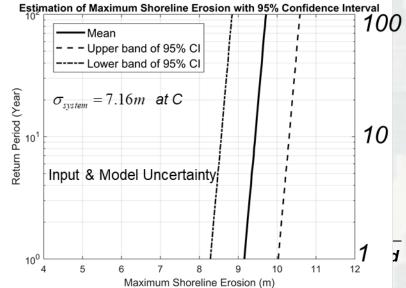


Uncertainty Estimation of Maximum Erosion at Point C



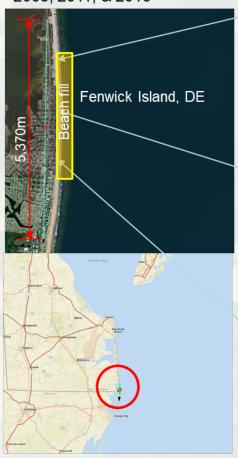


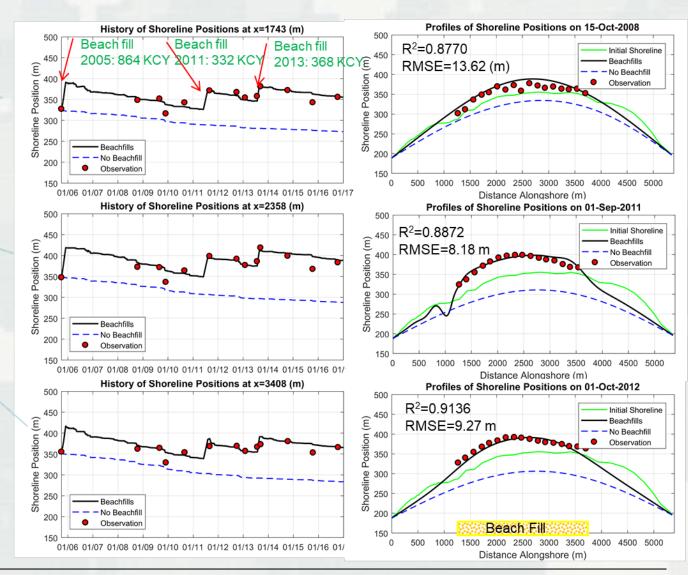




Long-term Shoreline Change in Fenwick Island, DE

- 12-year Shoreline Changes (2005-2017)
- Periodical beach fills:
 2005, 2011, & 2013



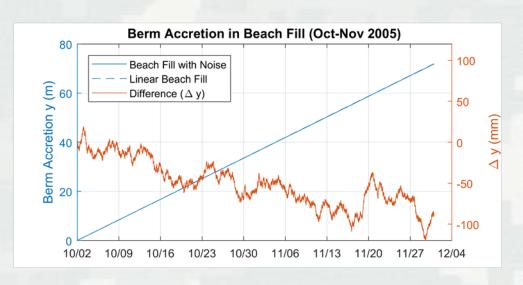


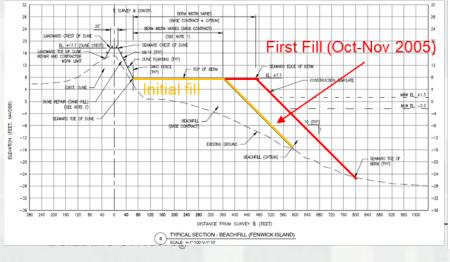
Uncertainty due to Beach Fill $(\Delta y(t))$

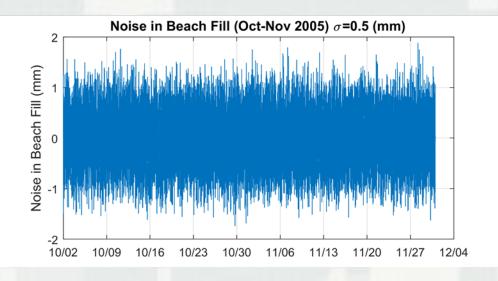
Beach fill (Δy) = Planned Beach Fill ($\overline{\Delta y}(t)$)+ White Noise

$$\Delta y(t) = \overline{\Delta y}(t) + N(0, \sigma^2)$$

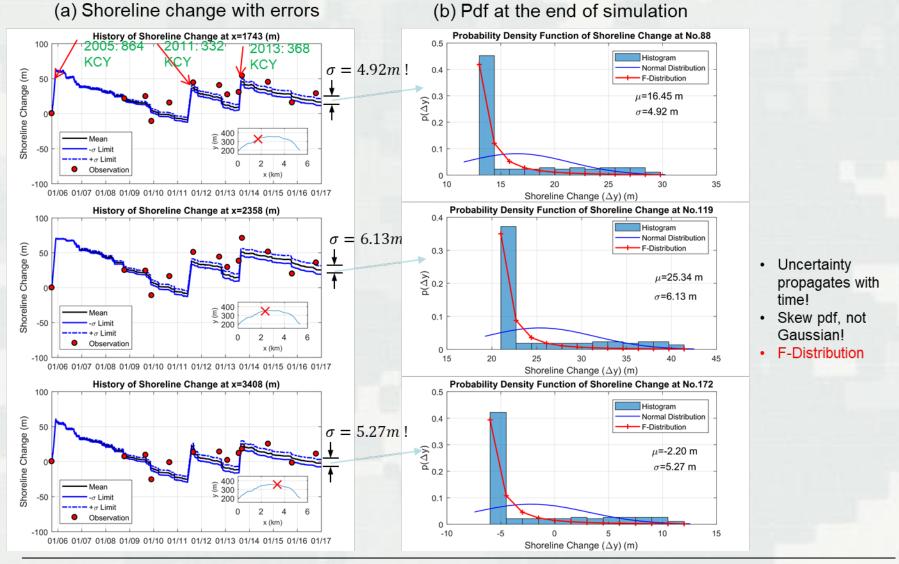




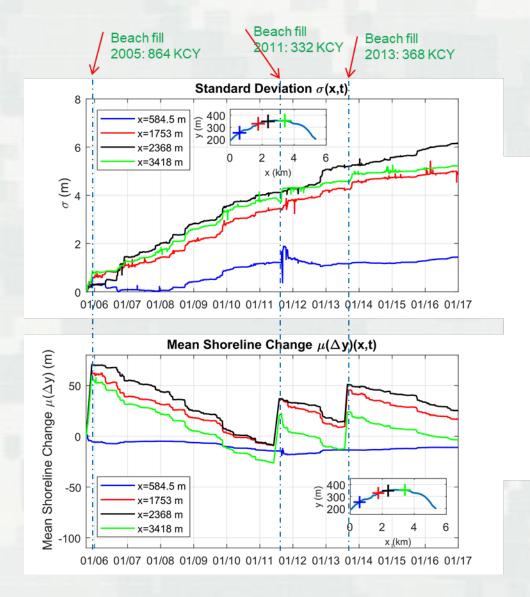


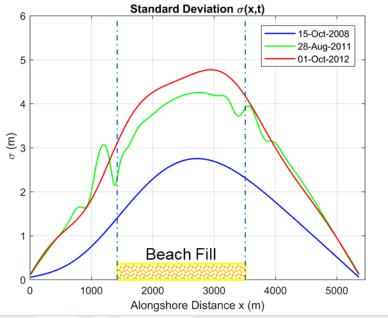


Variation of Shoreline Changes with Uncertainty in Beach Fill (1)

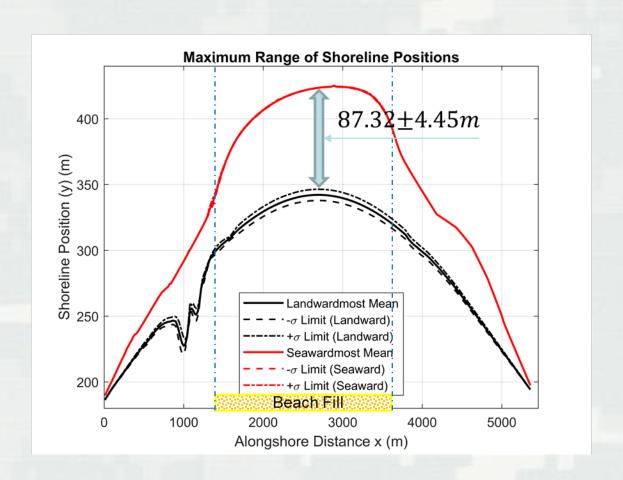


Errors/Uncertainty Propagating in Space (Beach) and Time





Maximum Range of Shoreline Changes: from Landwardmost to Seawardmost



Remarks

- GenCade-based Monte-Carlo (GenCade-MC) simulation provides a useful approach to assess uncertainty of shoreline change driven by waves.
- Maximum likelihood estimation of extreme shoreline changes predicts risk of erosion, which is essential for risk-based coast design.
- GenCade-MC is applicable to assess uncertainty of shoreline changes due to uncertainty in coastal protection practices (e.g. beach fill, nourishment).
- Further investigation of uncertainties by other factors (model parameters, boundary conditions, etc.) will be done.

Thank you for your attention!

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