

Analysis of Idealized Nearshore Berm Evolution using CMS

Brian McFall, Douglas Krafft, Mitchell Brown, Cody Johnson

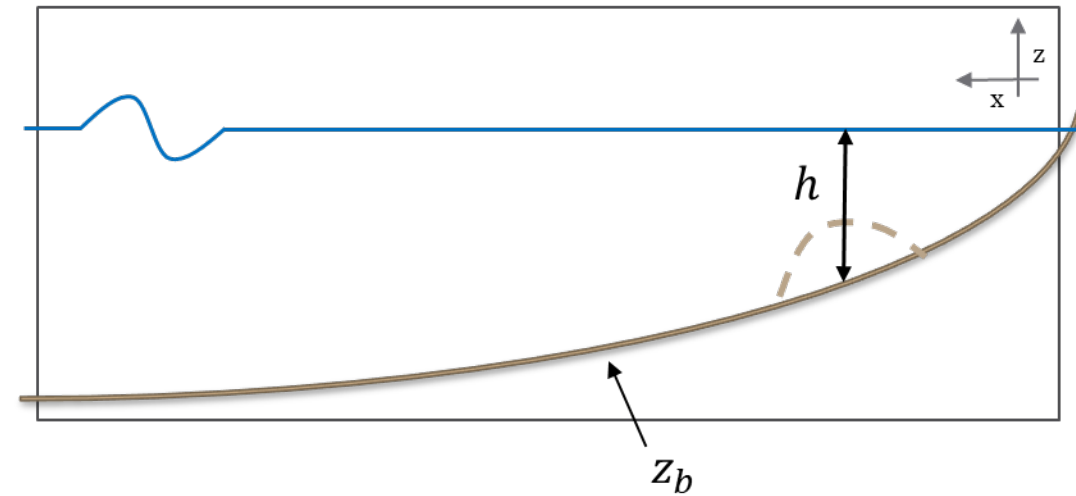
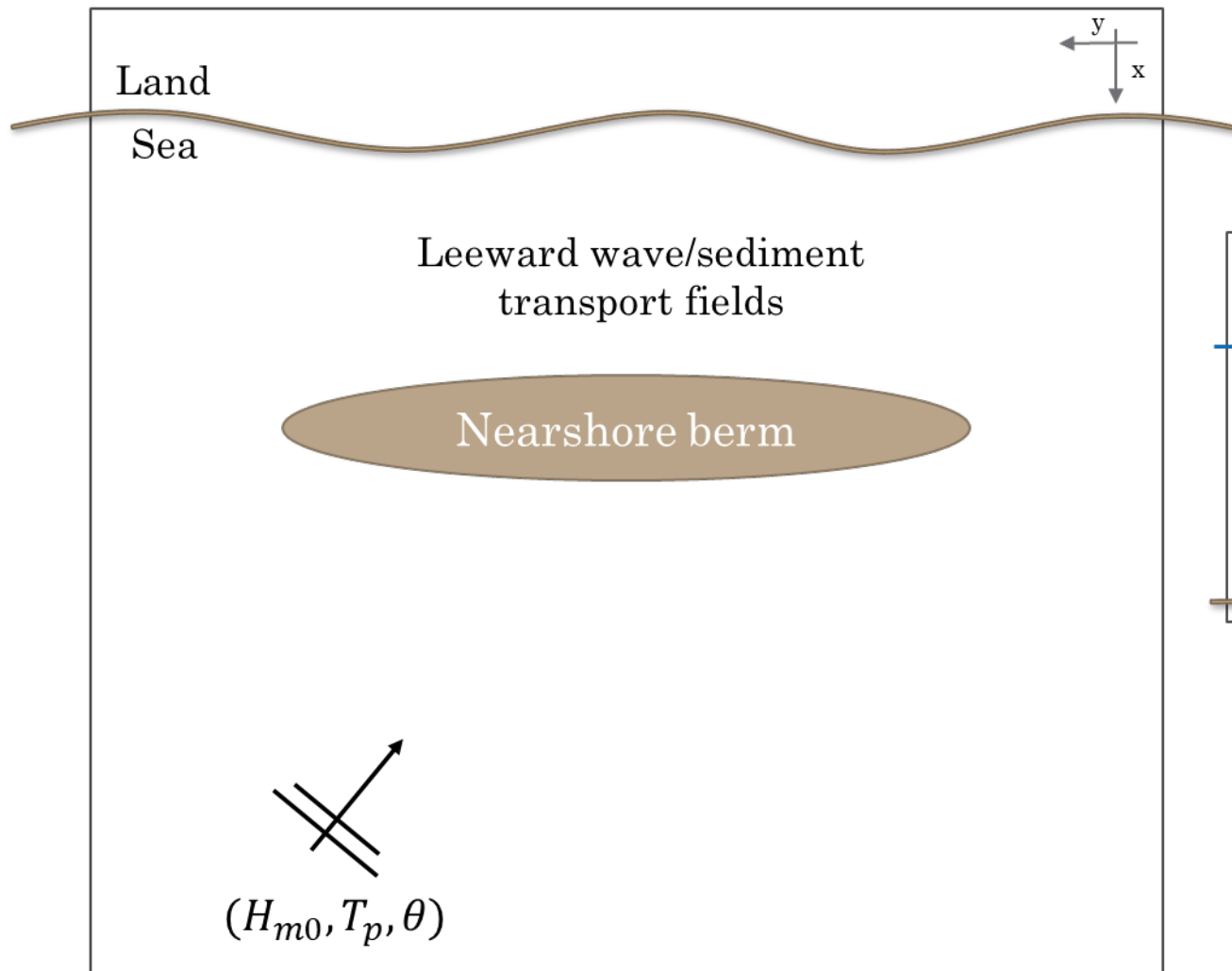
September 29th, 2020

Background

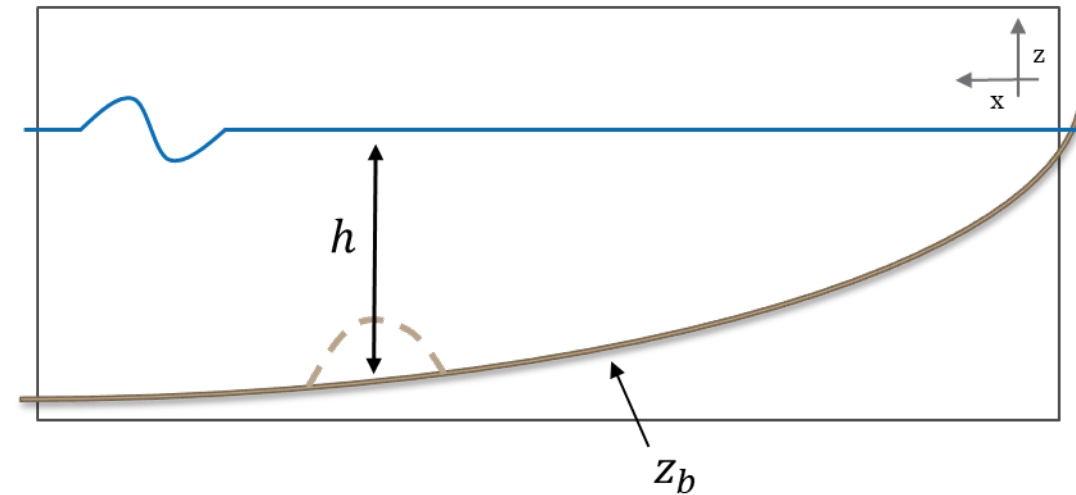
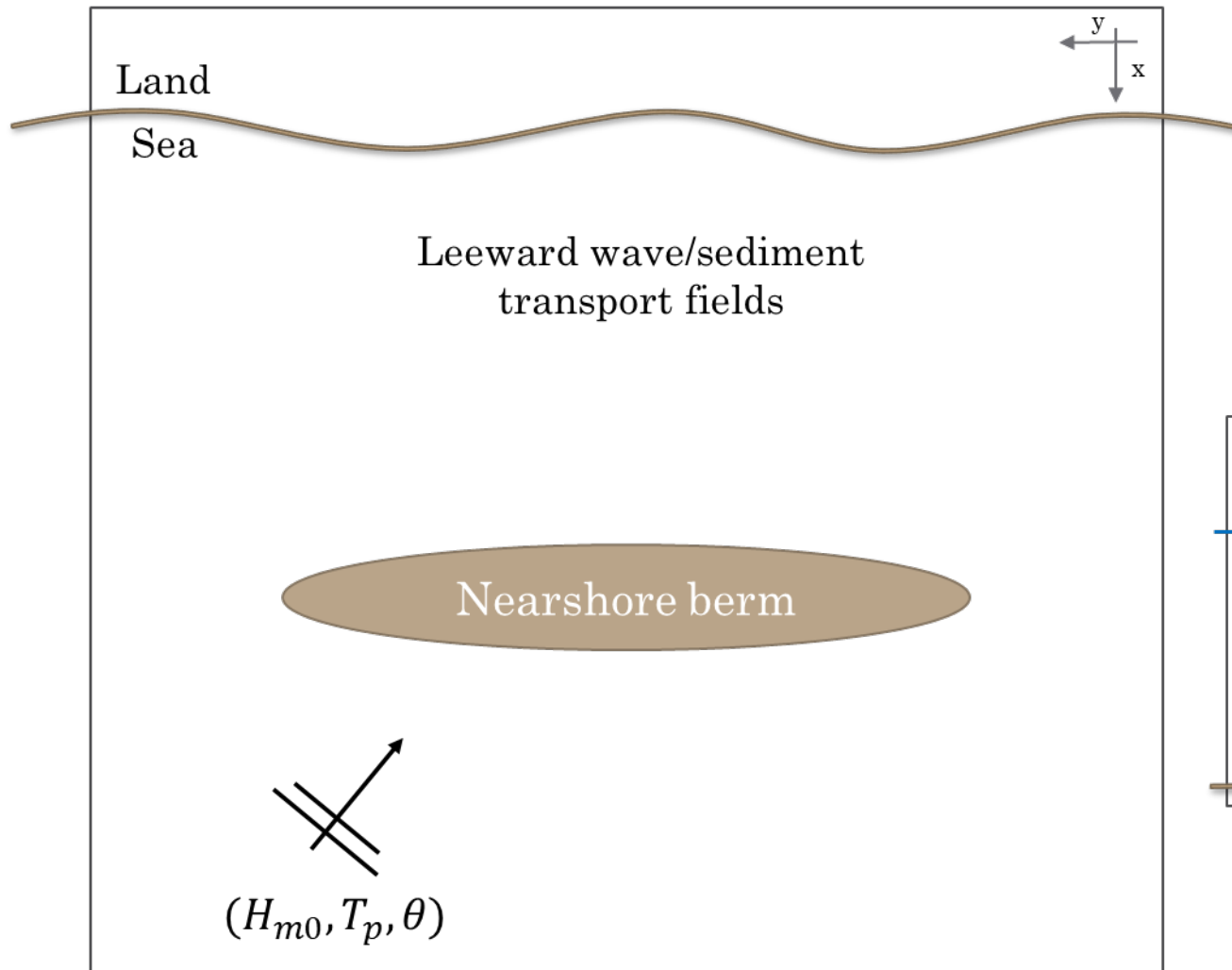
- The strategic placement of dredged sediment within the nearshore is an increasingly utilized practice to beneficially use dredge material.
- Placement geometry and depth affect shoreline response and sediment transport in the vicinity of the disposal site.
- Complex nearshore processes defy easy conceptualization, therefore model simplifications are made to highlight presumed 1st-order controls/effects.
- **Project Goal:** Quantify wave attenuation and sediment transport/morphodynamics under idealized conditions to provide a high-level understanding of placement geometry/depth.

Ultimately, provide guidance for the beneficial use of dredge material to O&M in the field.

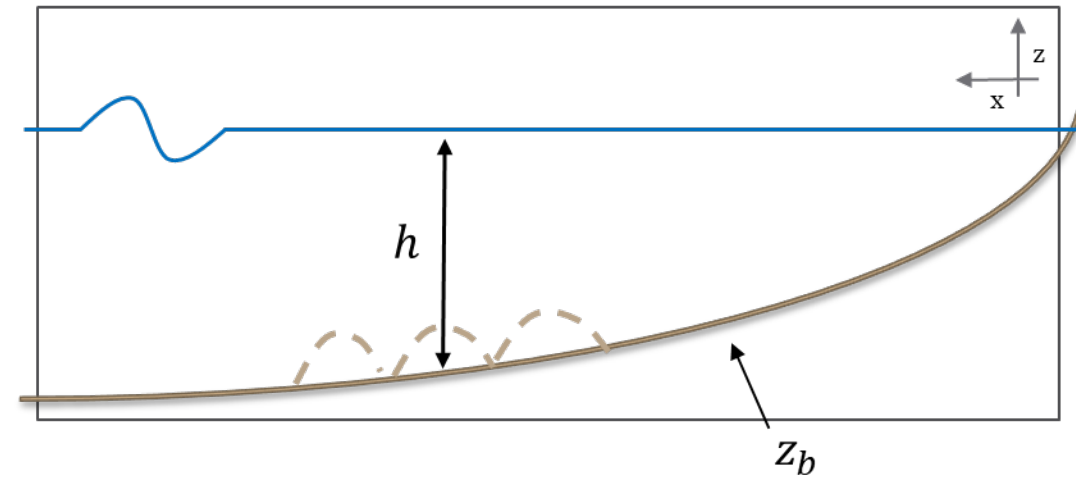
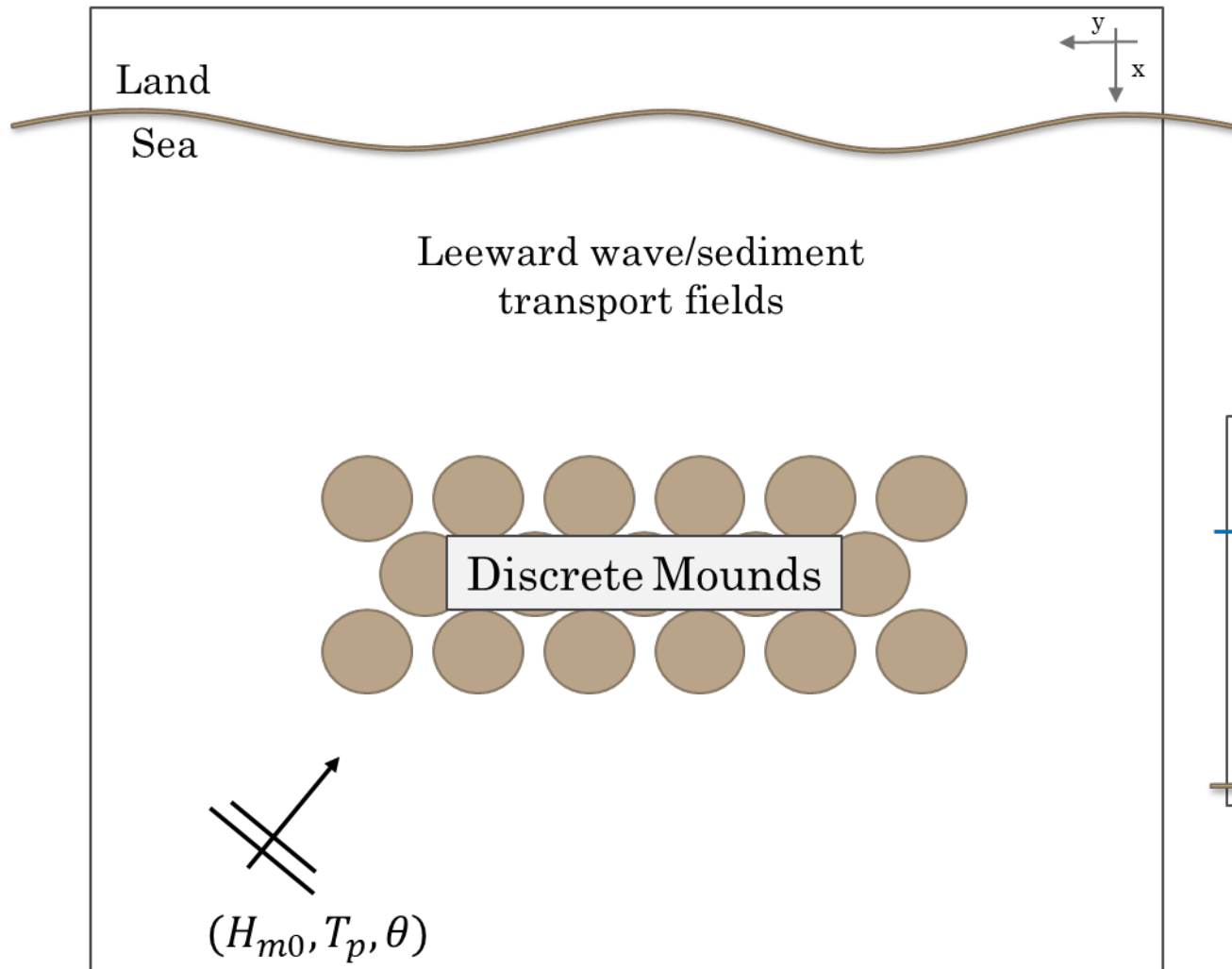
Idealized problem

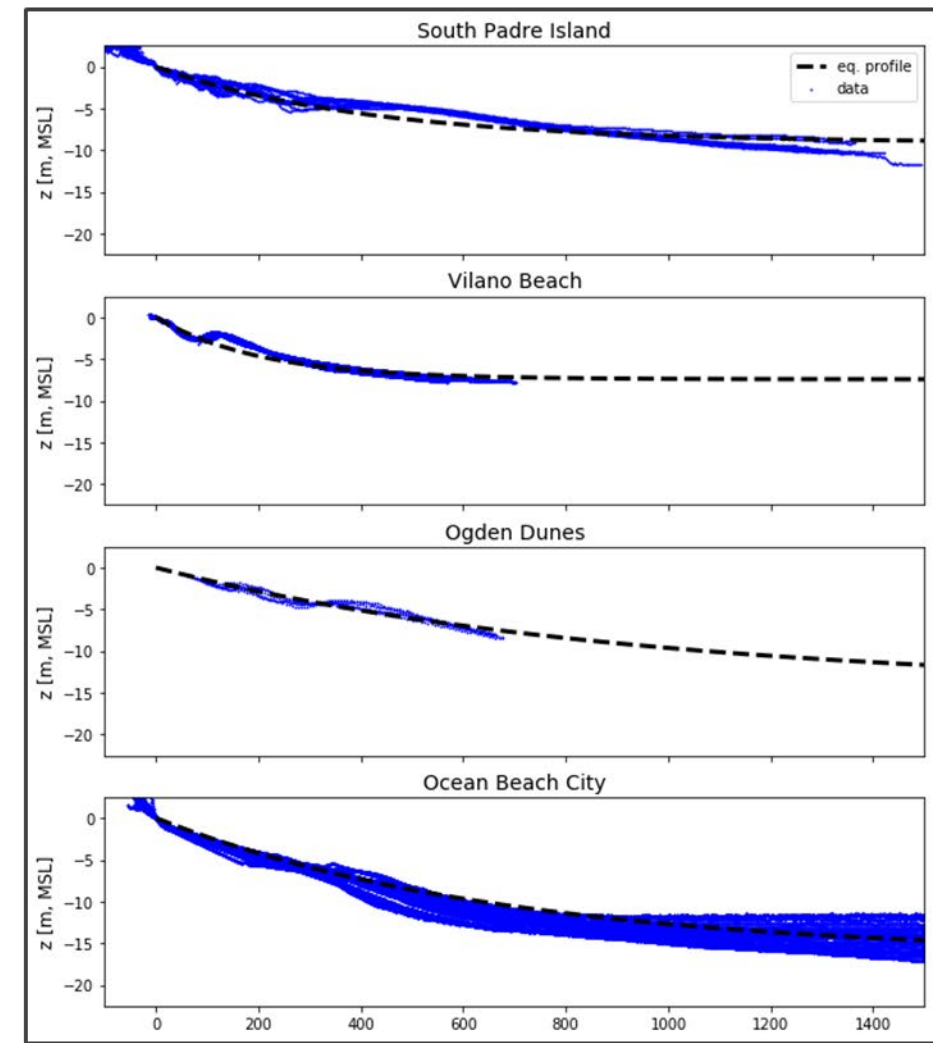


Idealized problem



Idealized problem





$$z_b = -h = \frac{-S_0}{k} (1 - e^{-kx})$$

S_0 = Shoreline slope

k = Profile decay coefficient

McFall, B. C. (2019). The Relationship between Beach Grain Size and Intertidal Beach Face Slope. *Journal of Coastal Research*, 35(5), 1080–1086.

Komar, P. D., & McDougal, W. G. (1994). The analysis of exponential beach profiles. *Journal of Coastal Research*, 10(1), 59–69.

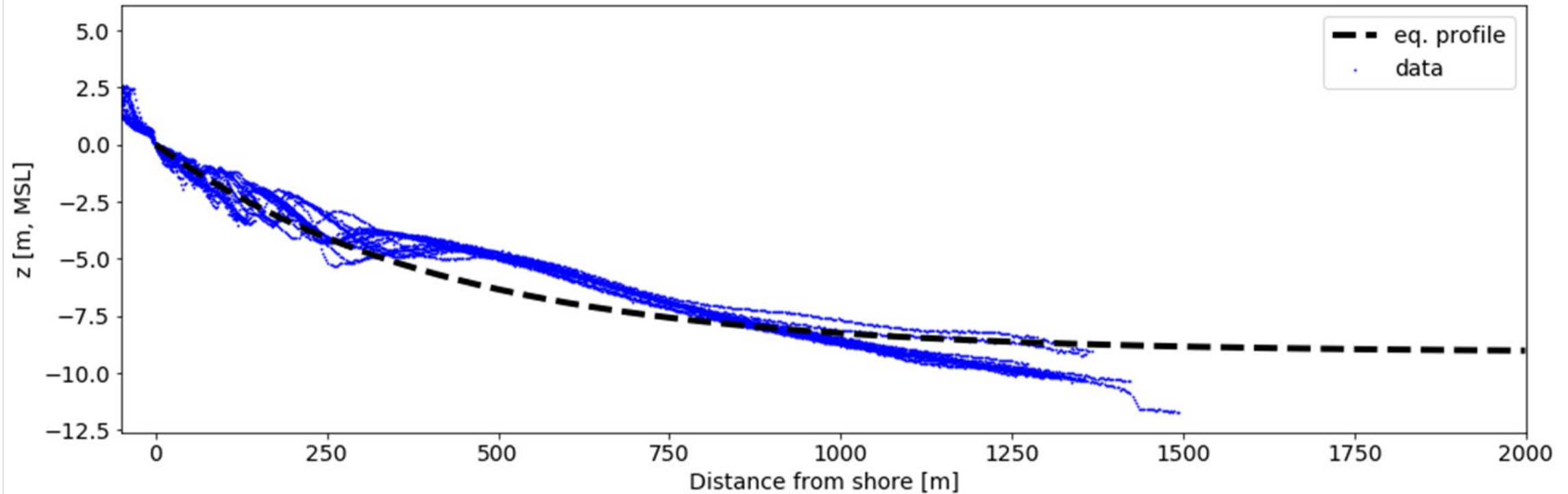


$$z_b = -h = \frac{-S_0}{k} (1 - e^{-kx})$$

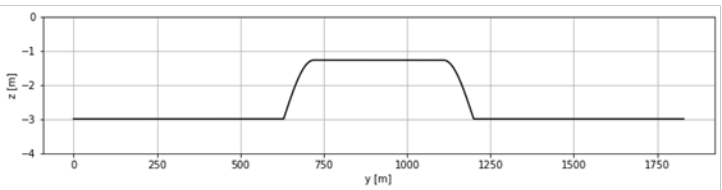
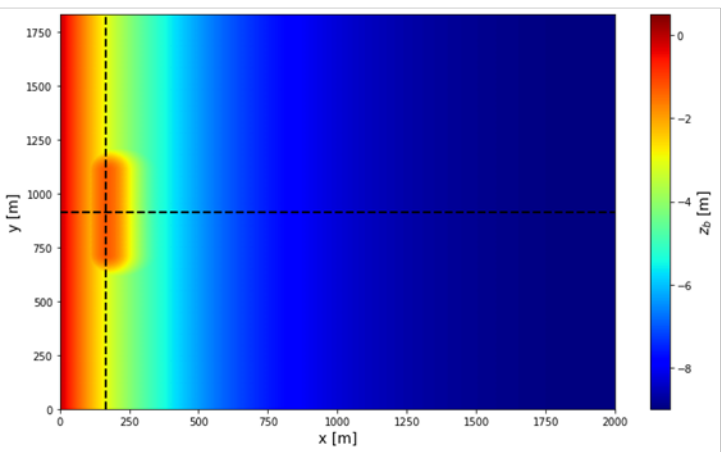
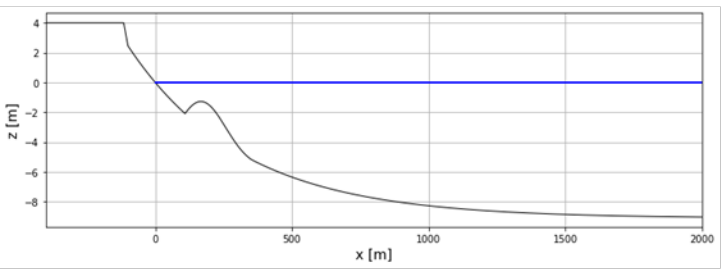
$$S_0 = 0.022$$

$$k = 0.002$$

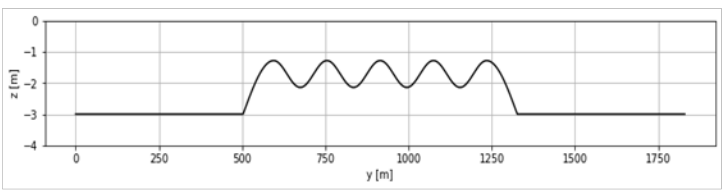
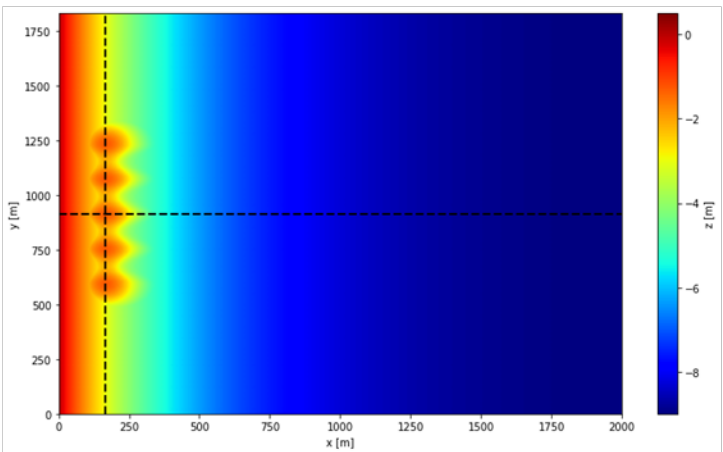
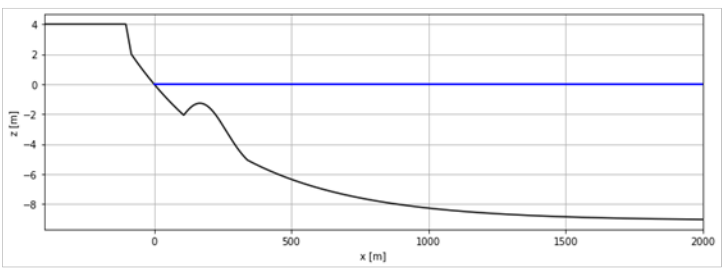
South Padre Island



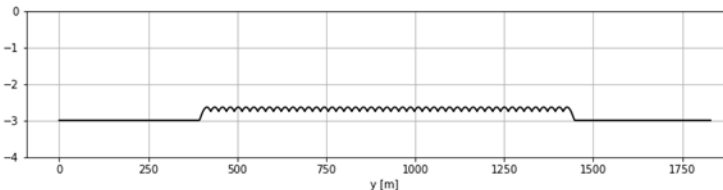
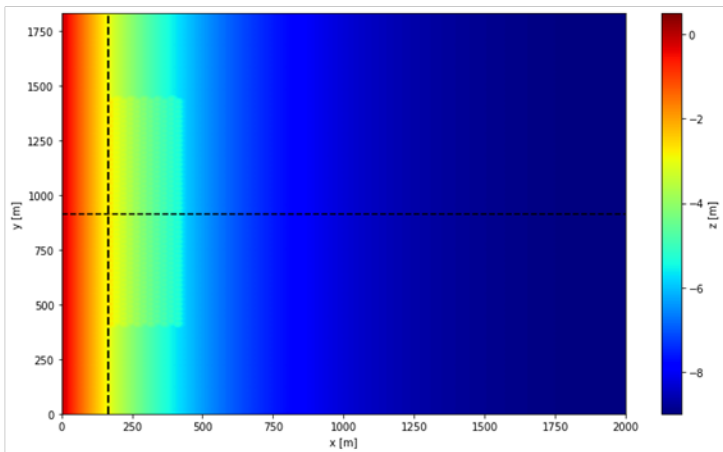
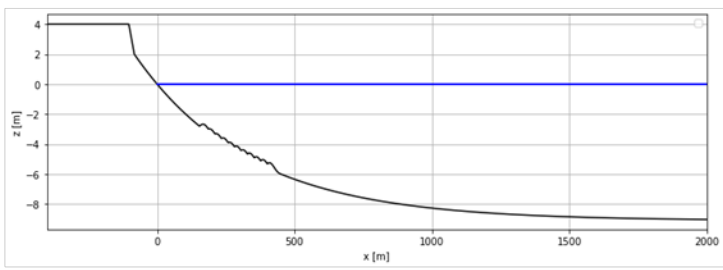
Linear Berm



Undulated Berm

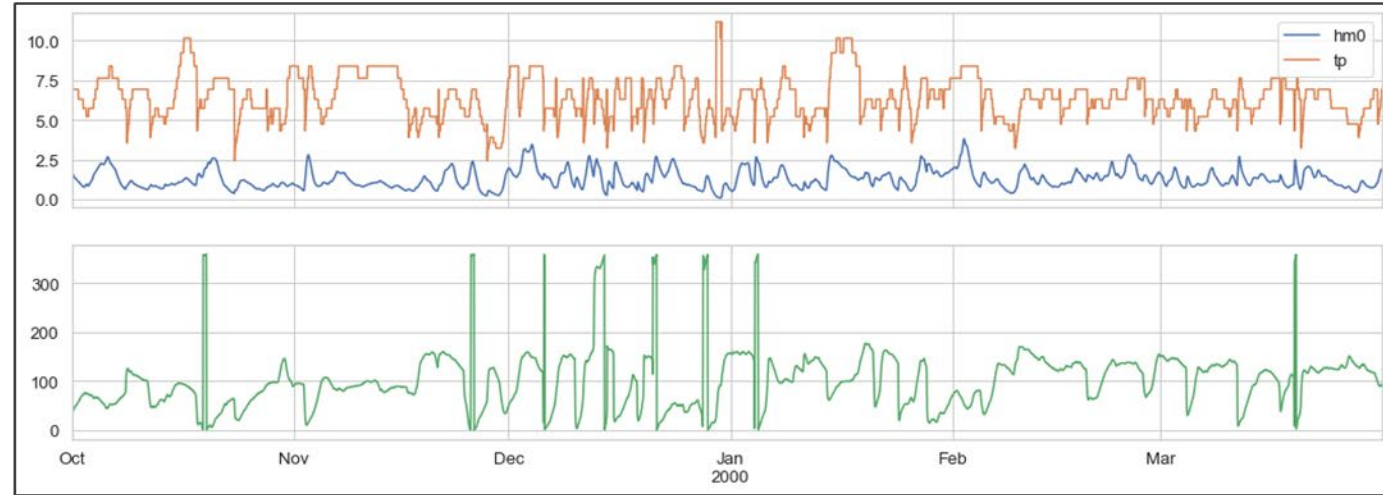


Discrete Mounds

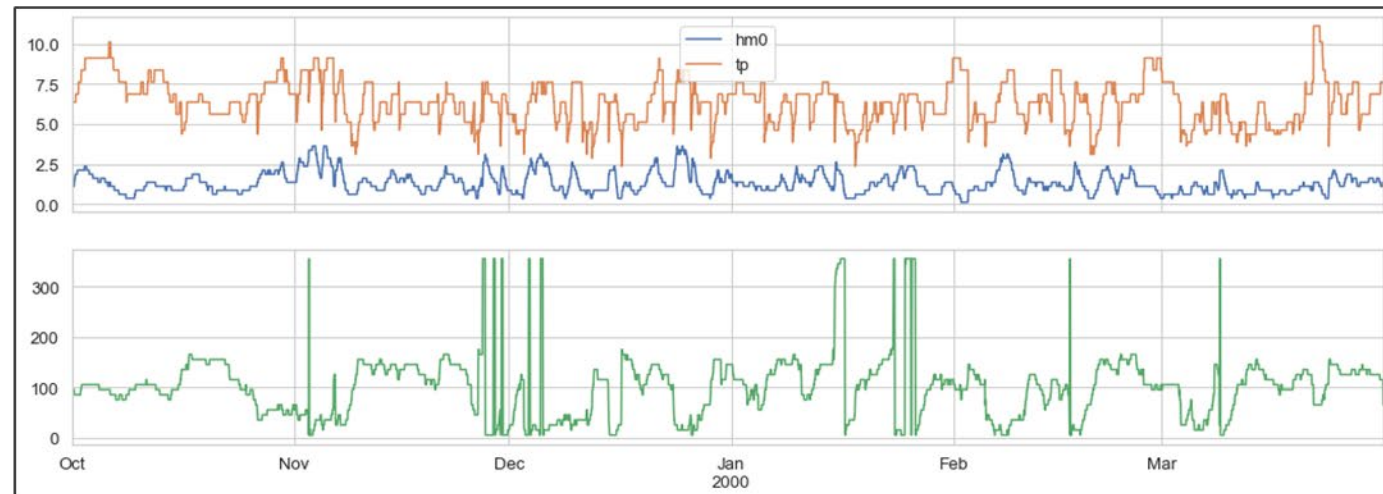


Markov Chain model

WIS data



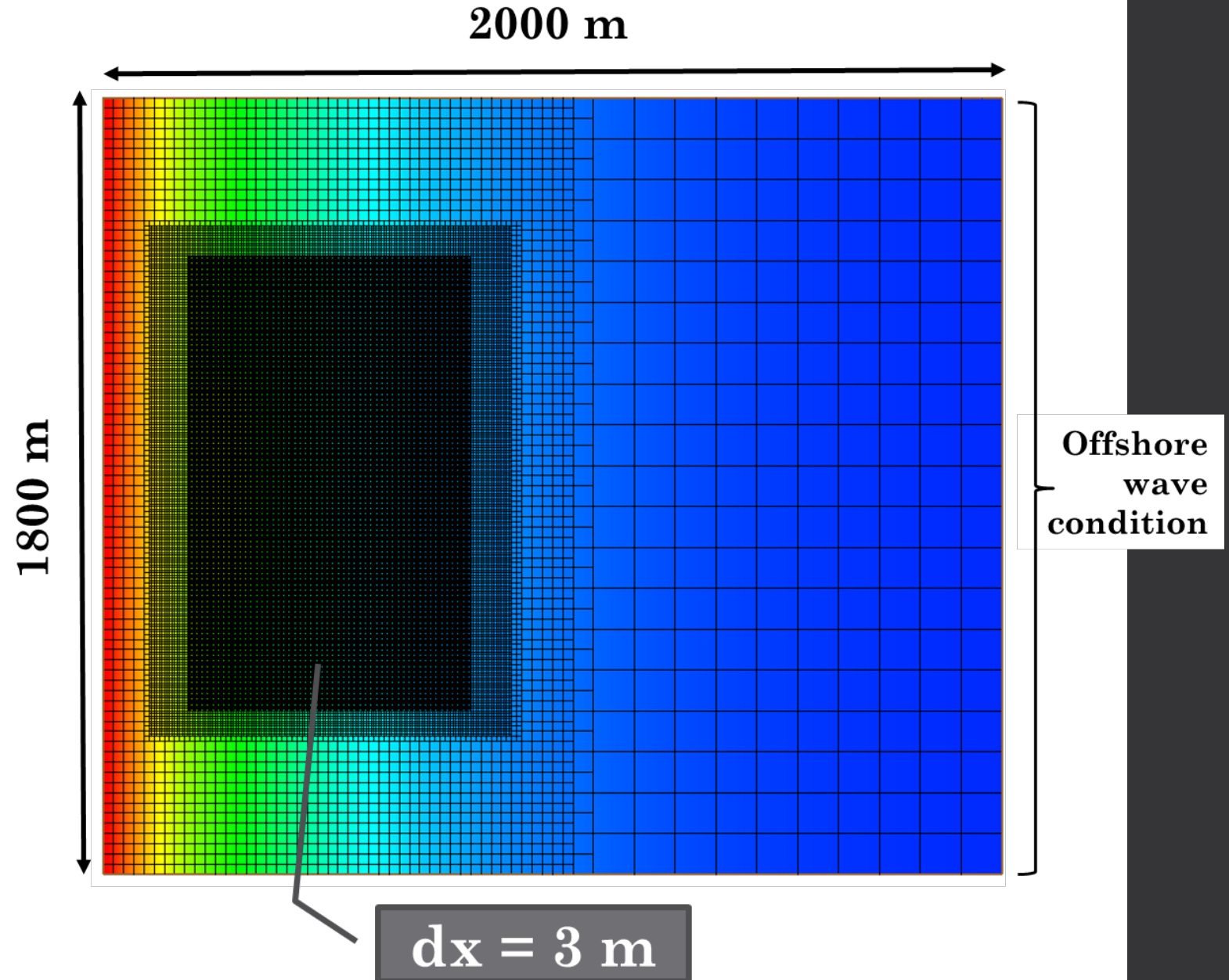
Synthetic time series



De Masi, G., Bruschi, R., & Drago, M. (2015). Synthetic metocean time series generation for offshore operability and design based on multivariate Markov model. *MTS/IEEE OCEANS 2015*

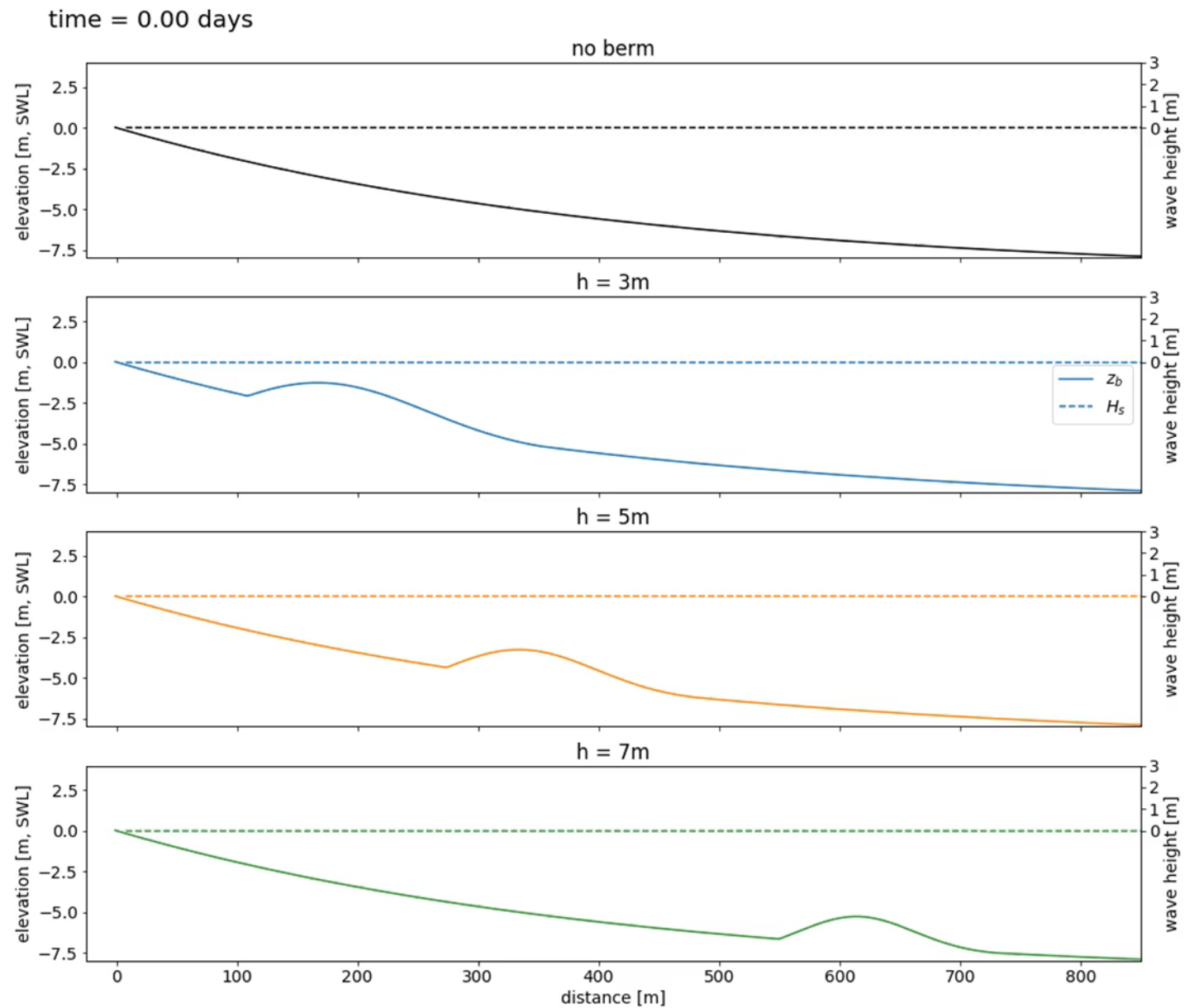
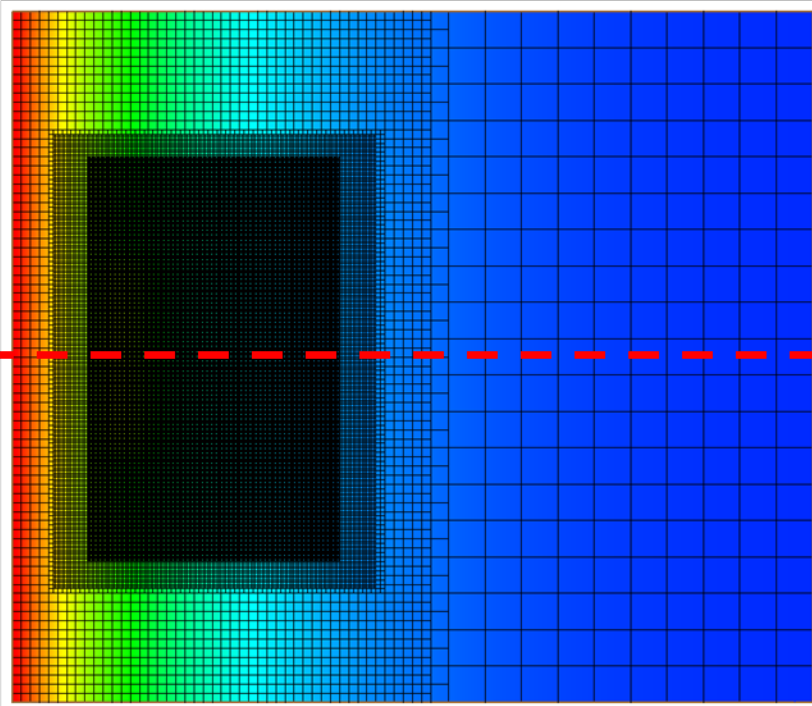
Coastal Modeling System (CMS)

- Coupled waves/flow
- Phase-averaged wave model
- 6 month simulation time
- Open boundary water levels pinched at zero
- LundCIRP sediment transport formula
- Uniform grainsize depending on case study

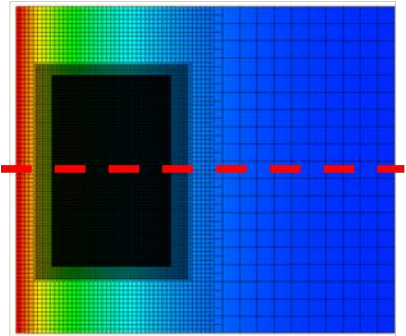


Linear Berm

Profile location



Profile location

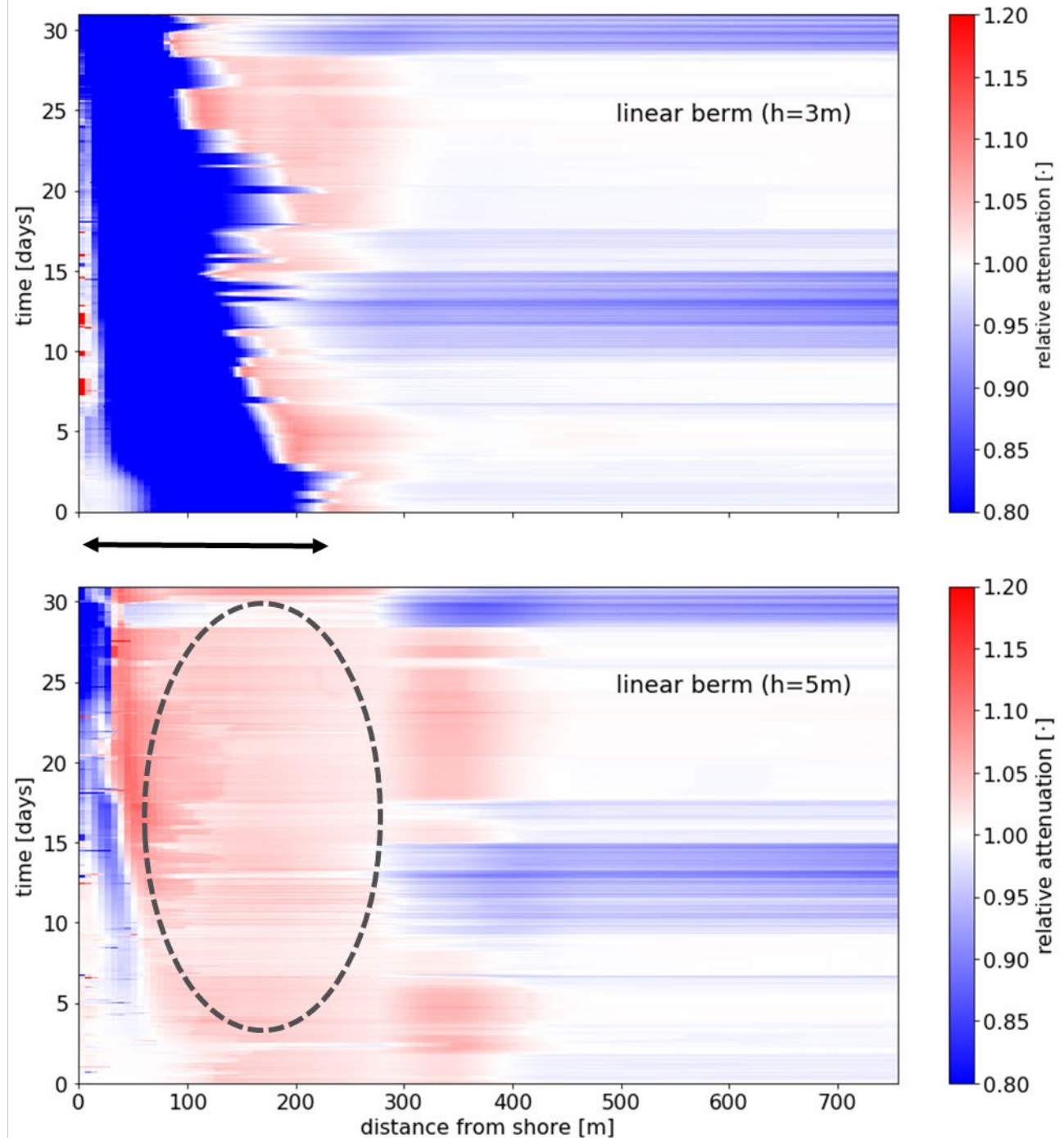


- Relative wave height

$$\alpha = \frac{H_s}{H_s^*}$$

H_s = Significant wave height
 H_s^* = Wave height in control case

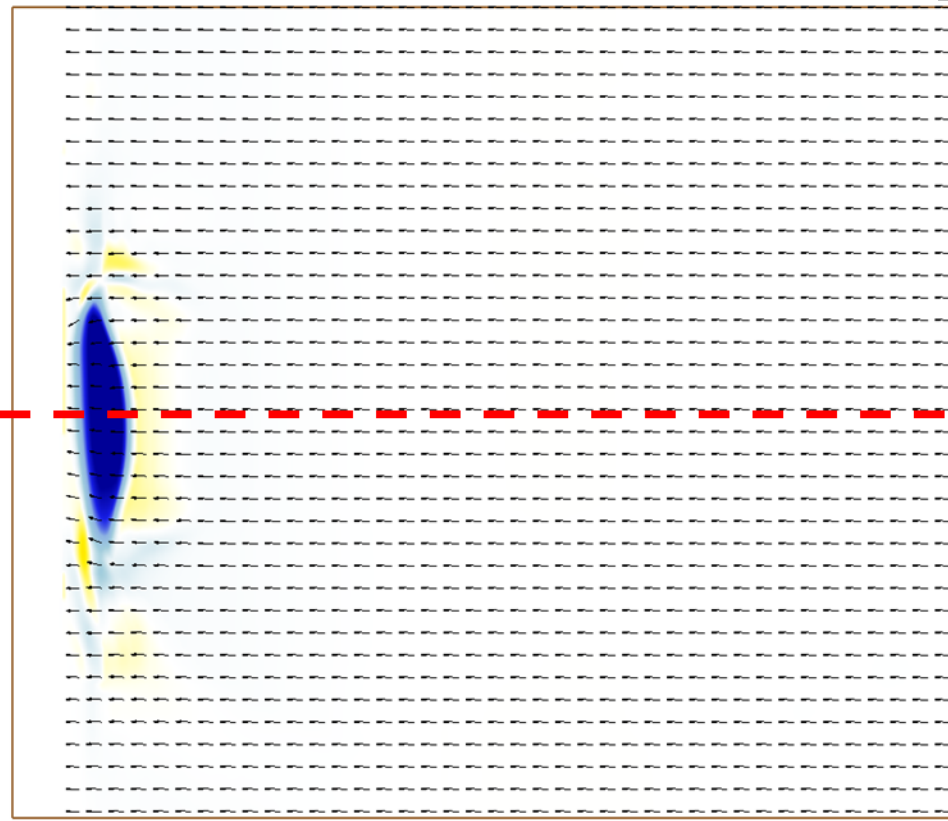
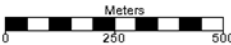
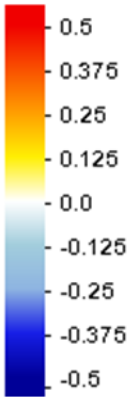
- Increased wave energy dissipation in surf zone for $h=3\text{m}$ simulation
- Amplification of wave energy leeward of berm for $h=5\text{m}$



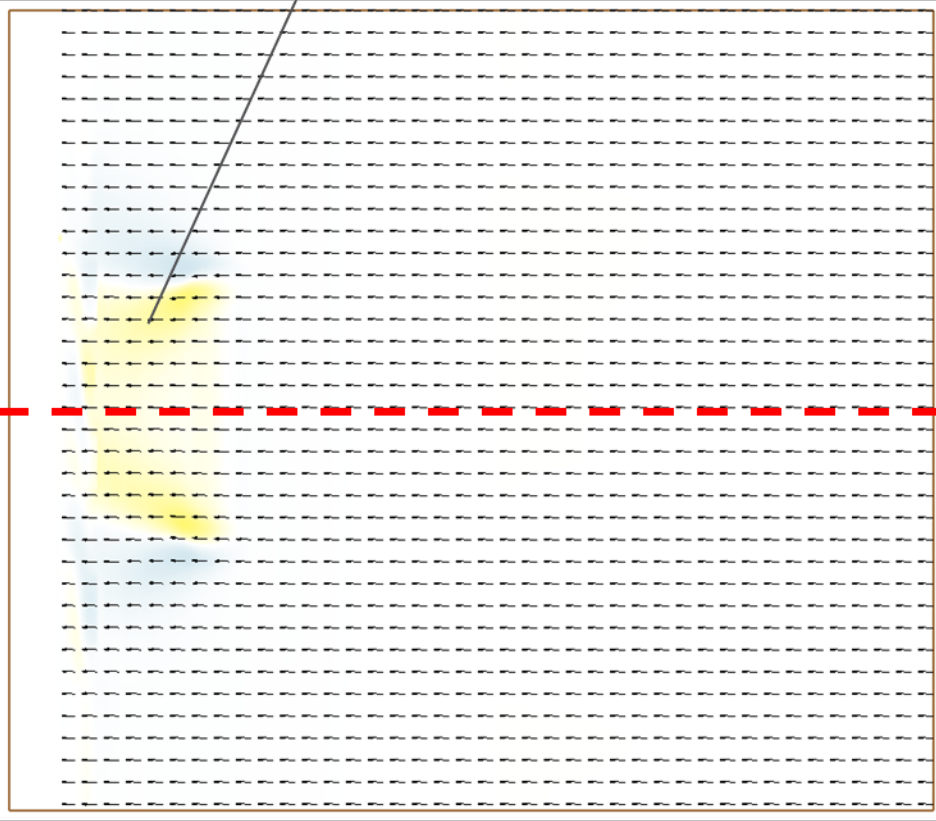
$\Delta H_s = H_s - H_s^*$

Simulation time = 8 days

Quadtree wave_height_diff_h3_minus_base 10/8/1999 7:00:00 PM



Linear berm h=3 m

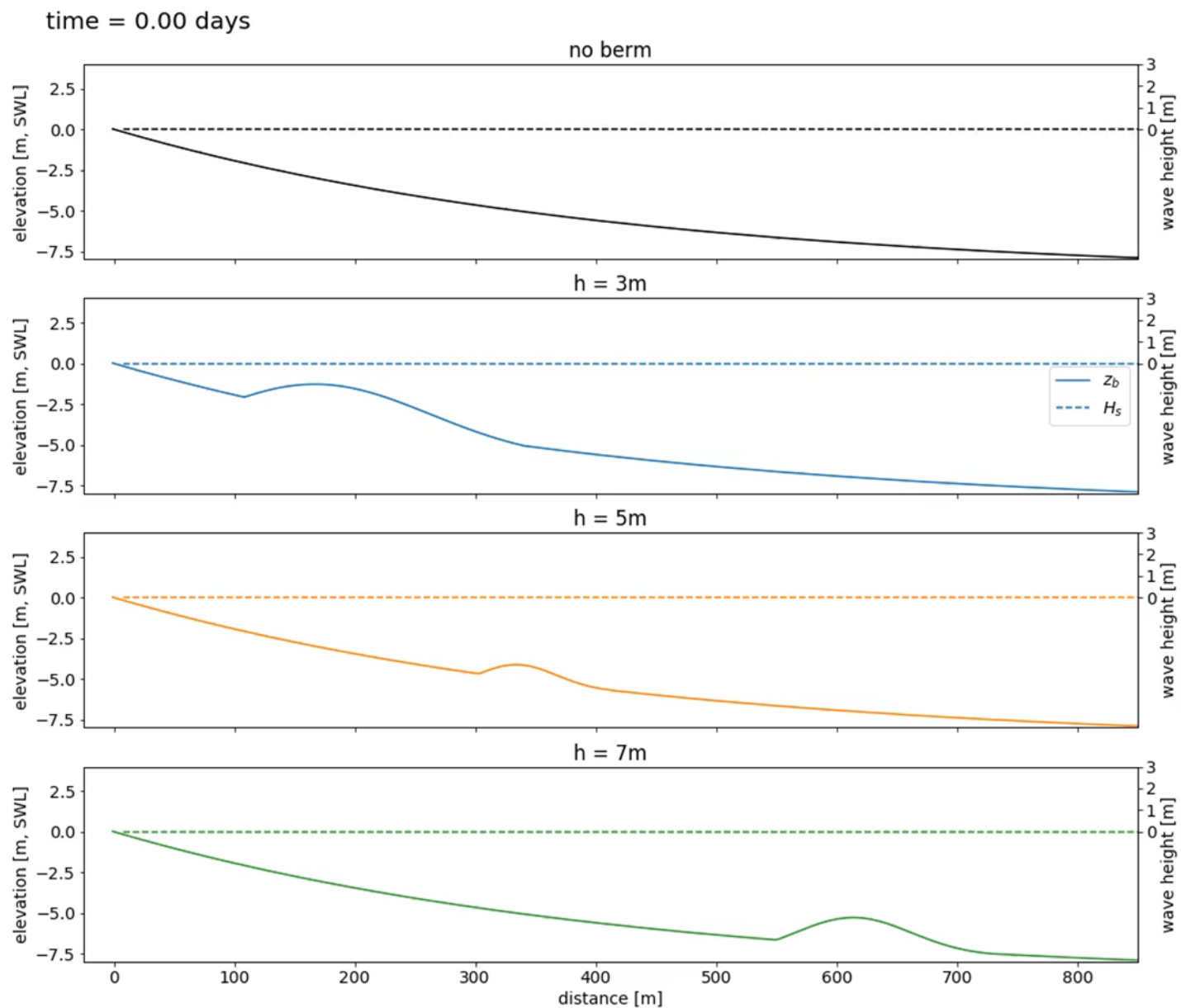
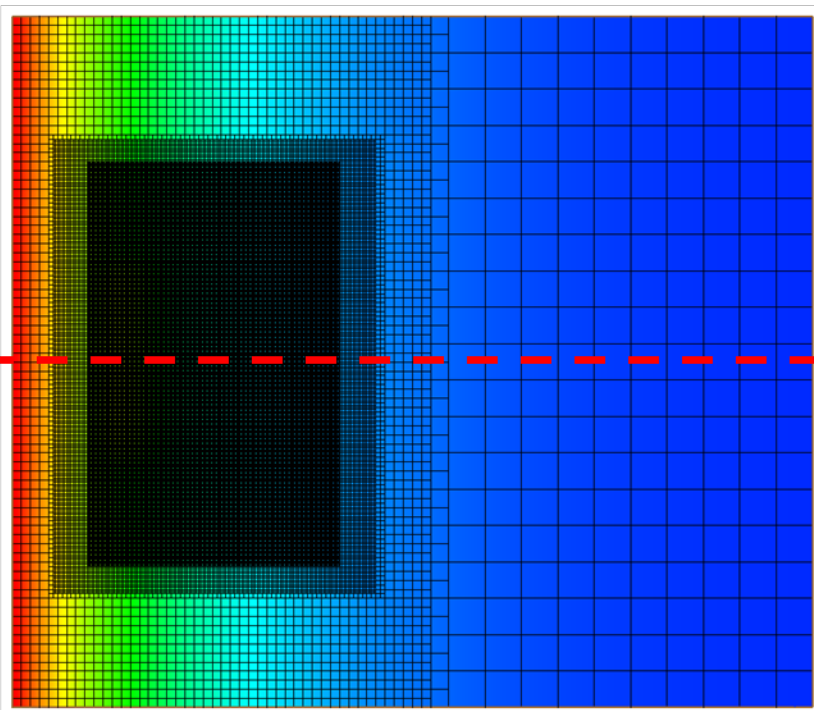


Linear berm h=5 m

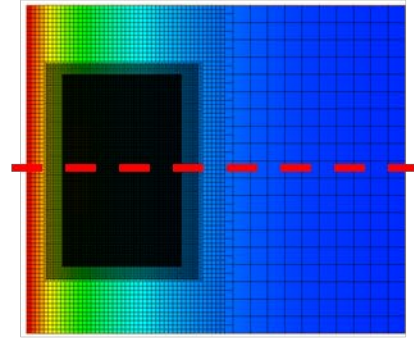
Wave diffraction (?)
leeward of berm

Undulated Berm

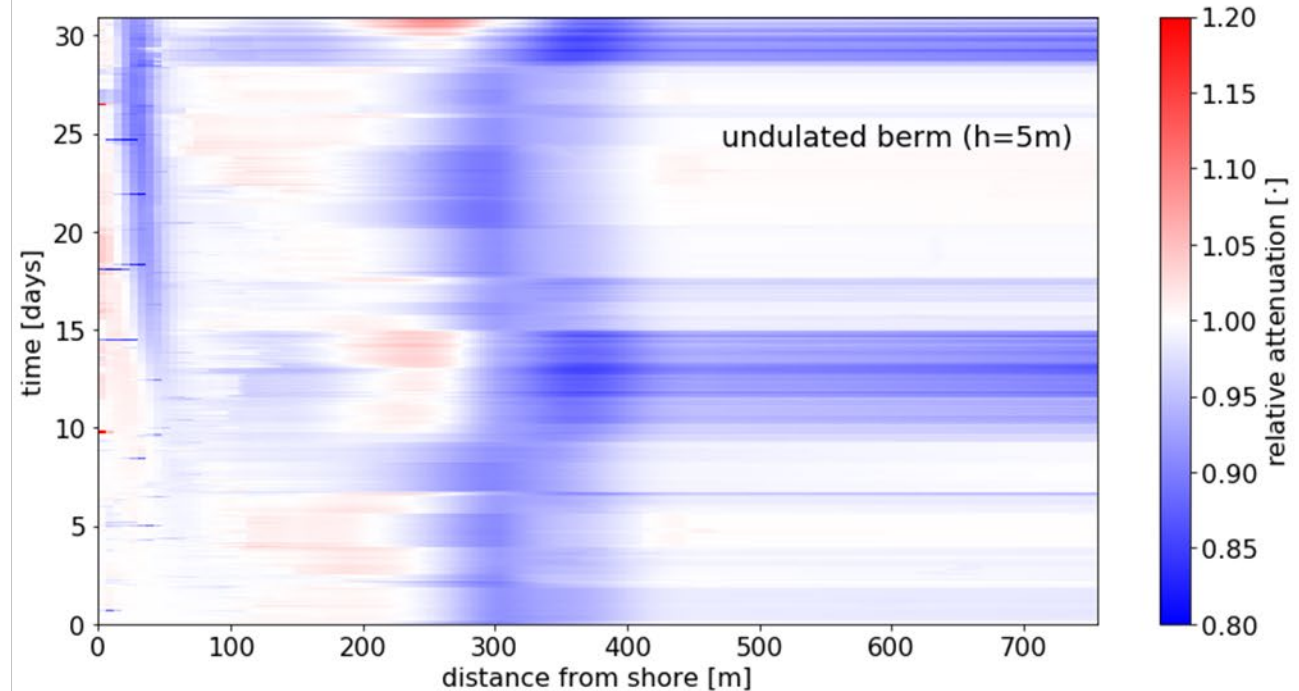
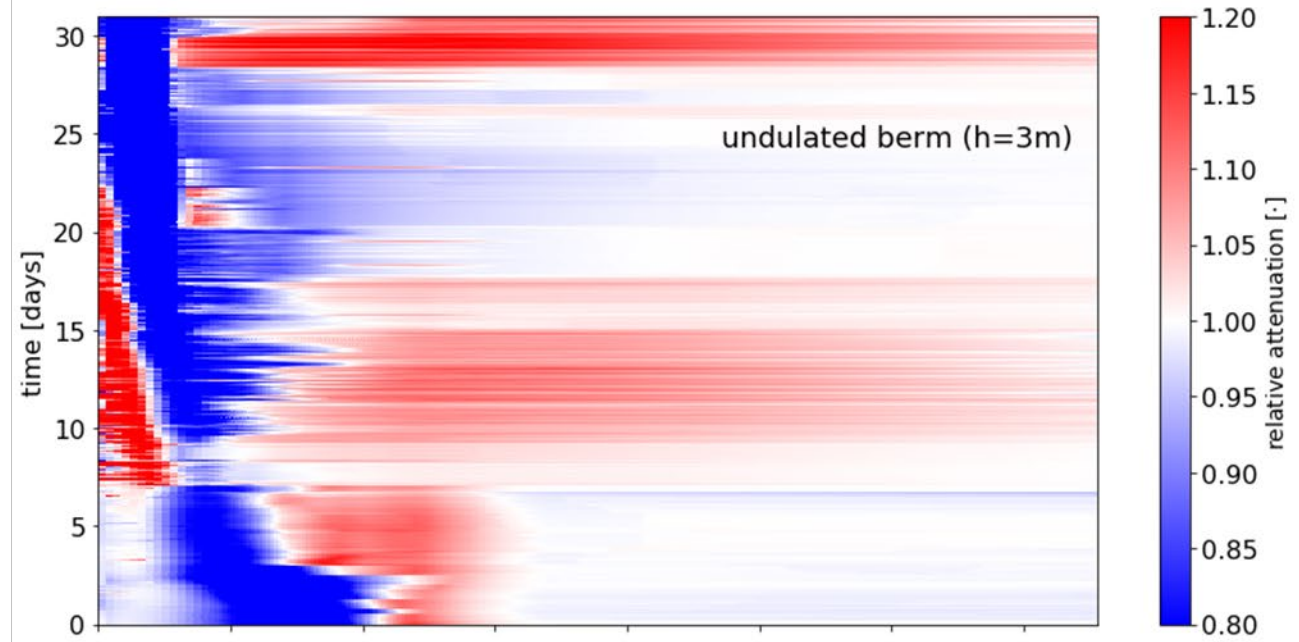
Profile location



Profile location



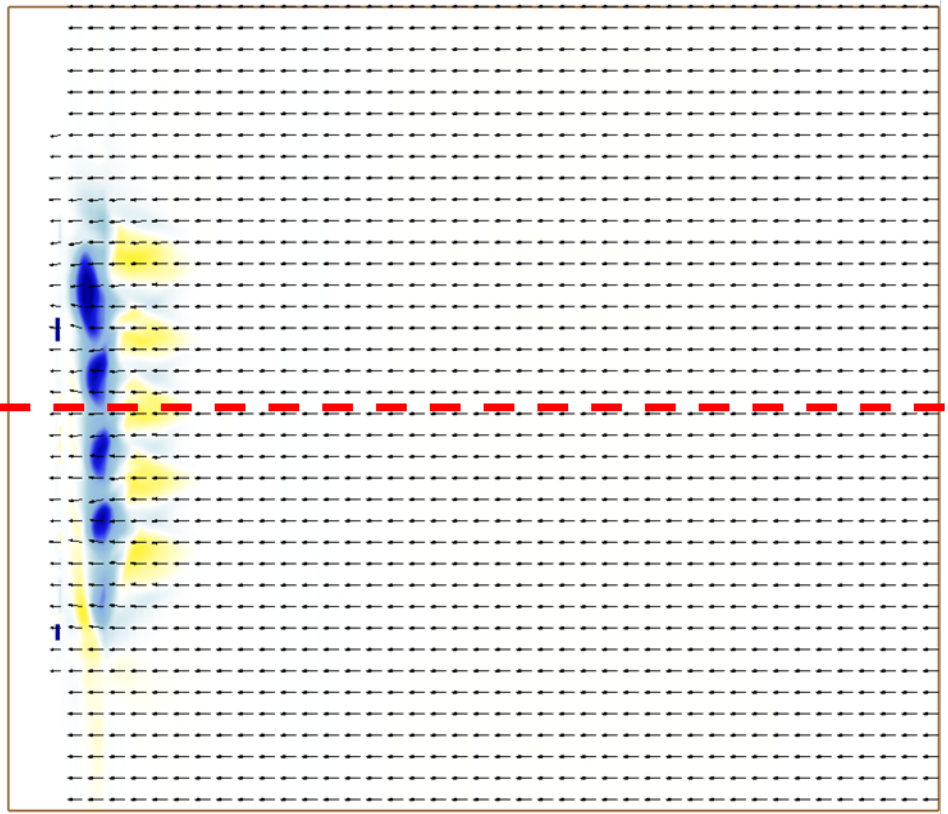
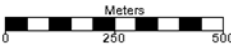
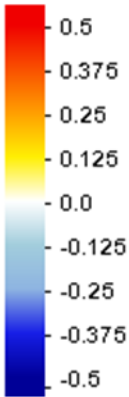
- Less energy dissipation in surfzone
- Also, less amplification of wave energy leeward of berm for $h=5\text{m}$



$$\Delta H_s = H_s - H_s^*$$

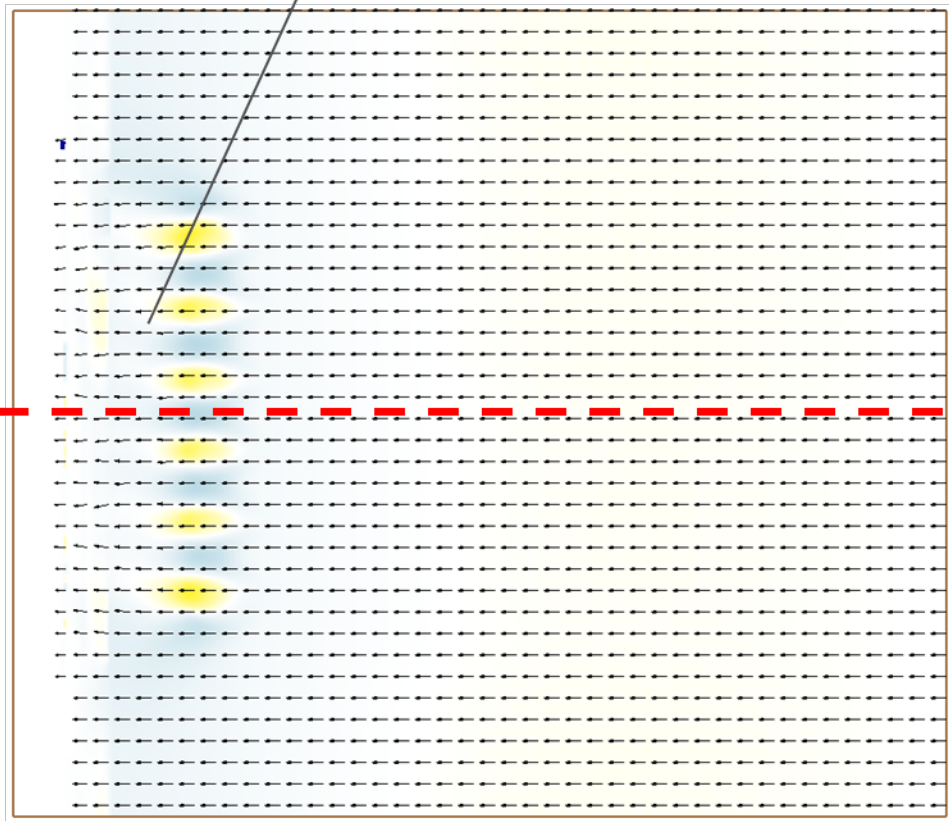
Simulation time = 8 days

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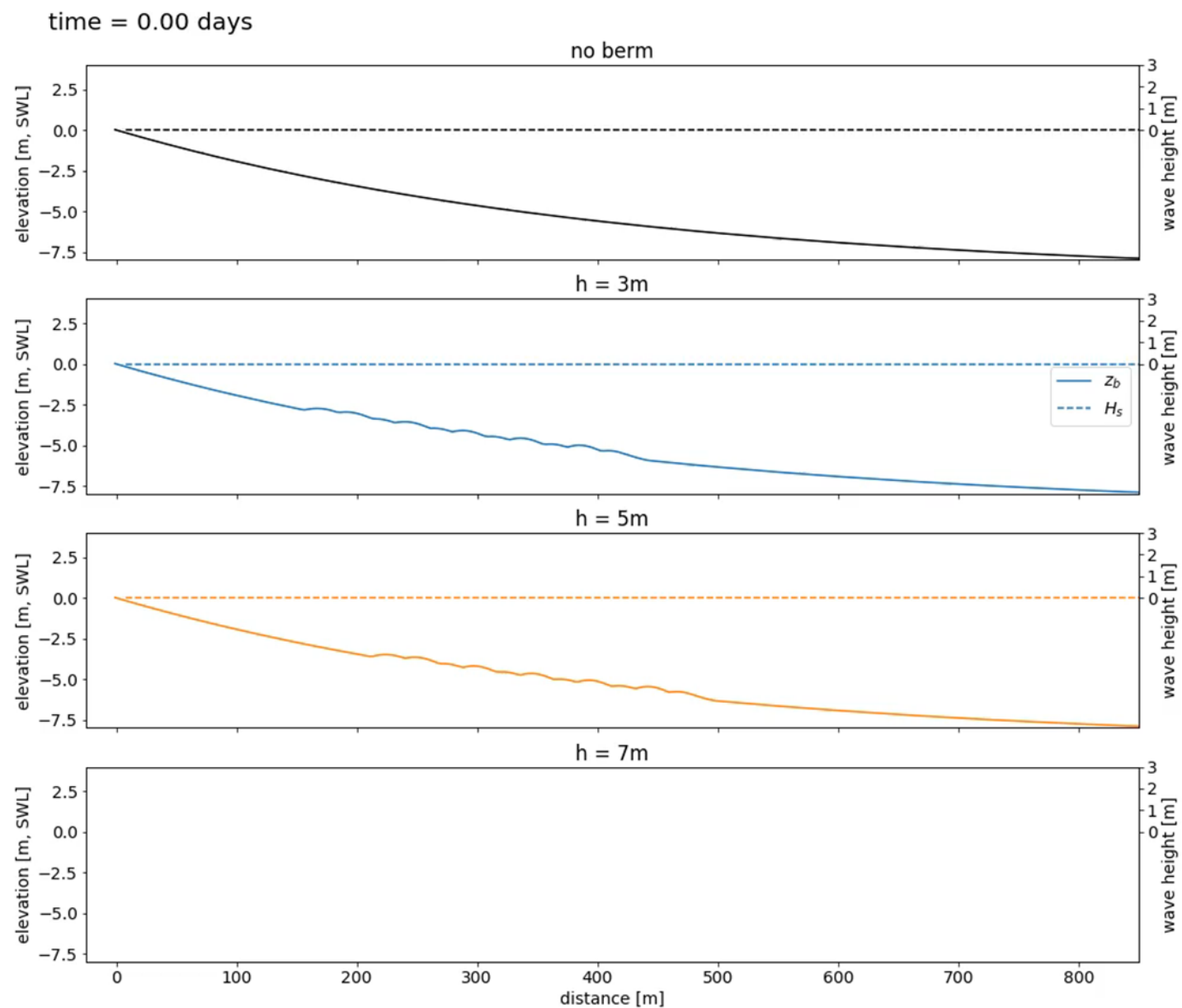
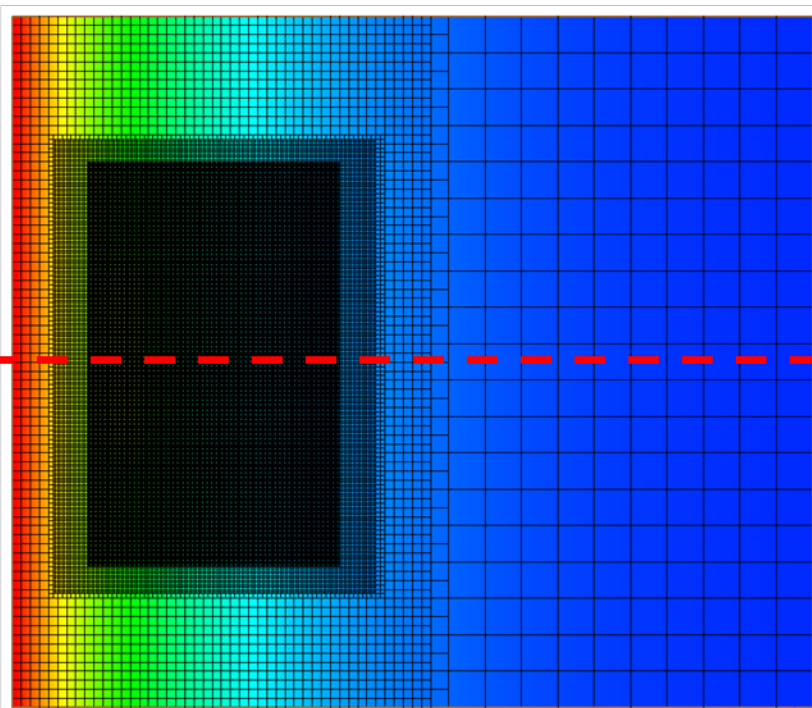
Undulated berm h=3 m

No diffraction
leeward of berm



Undulated berm h=5 m

Profile location

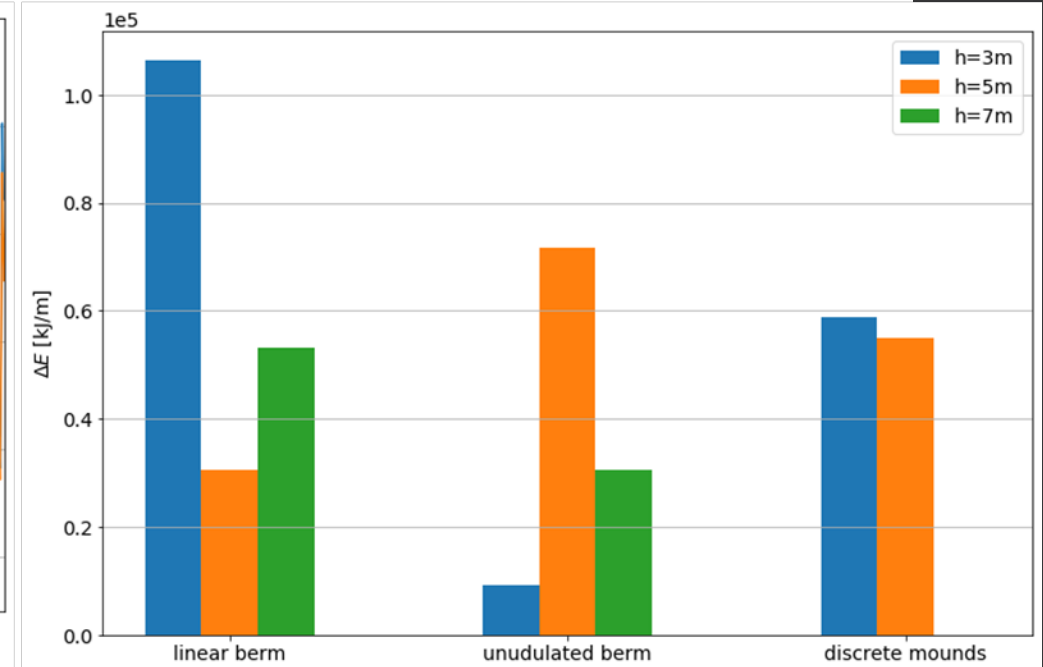
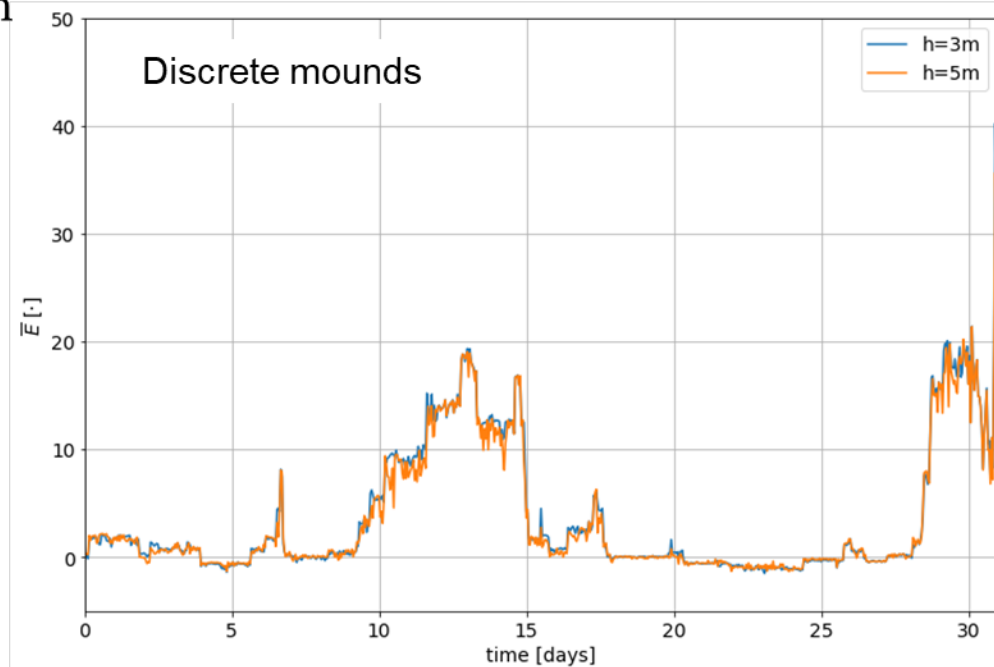
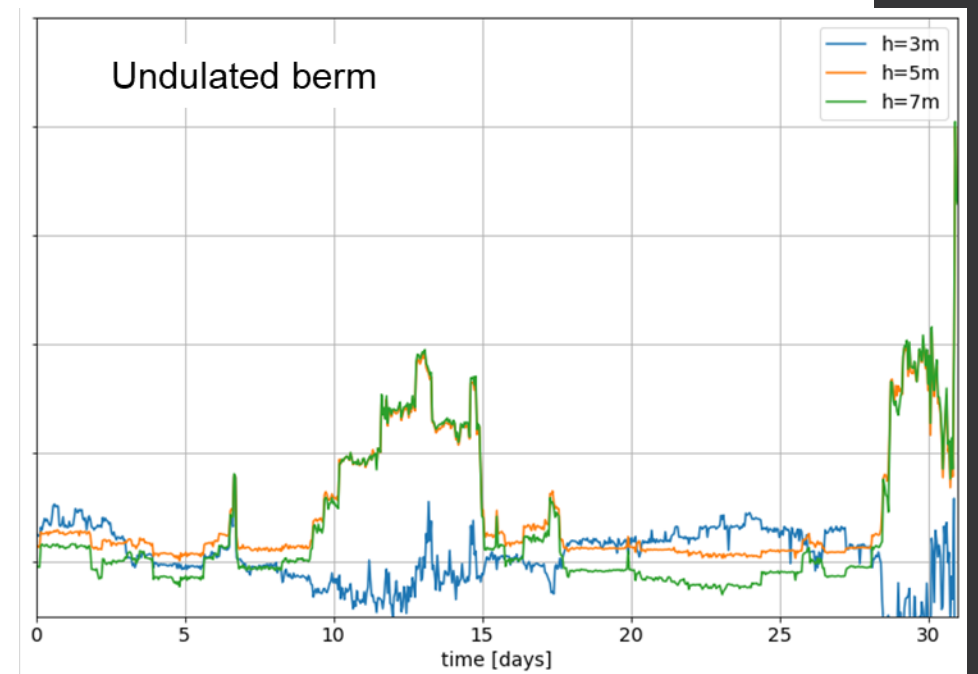
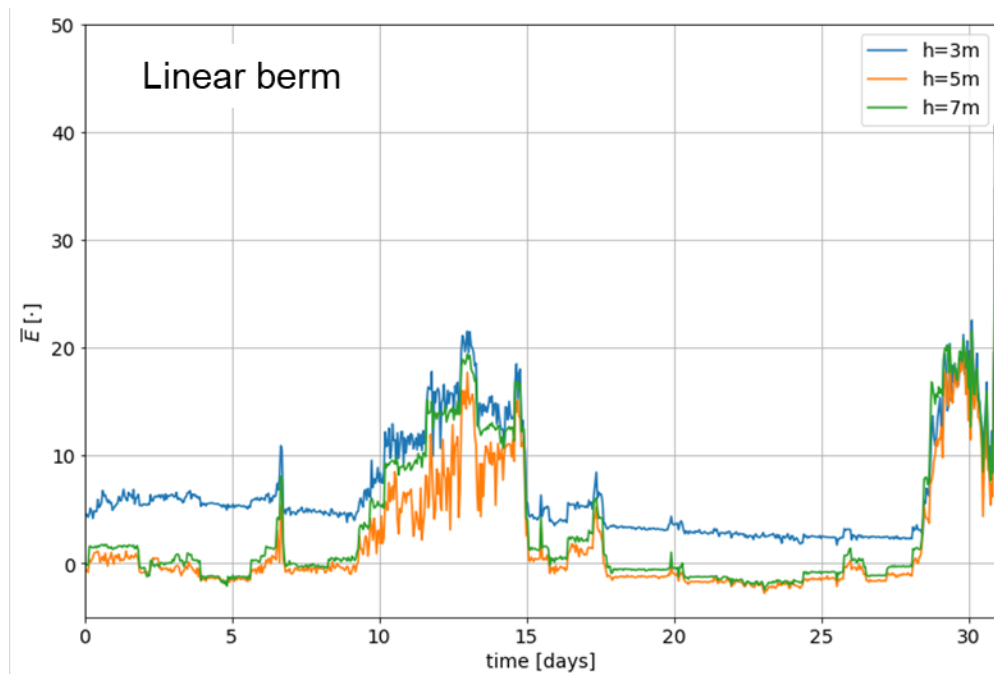


$$E = \frac{1}{8} \rho g H_s^2$$

$$\Delta E = E^* - E$$

$$\bar{E} = \frac{\int \Delta E dx}{\int E^* dx}$$

E^* = Energy from
control case



Future work

- Concise method to quantify, summarize, and communicate the results
 - Consider effects in 2D
- Analyze shoreline and profile accretion
- Inter-site comparison that considers on-shore/off-shore sediment transport depending on dissipative/reflective nearshore profile.

Thank you!