



EMPIRICAL & IDEALIZED
NUMERICAL MODELING OF VESSEL
WAKE

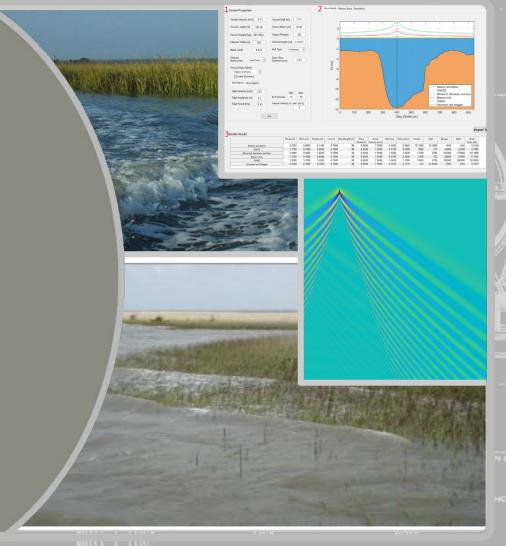
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Kathy Griffin

HQ Navigation Business Line Manager

Eddie Wiggins

Technical Director





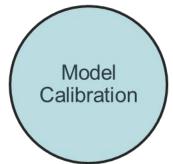




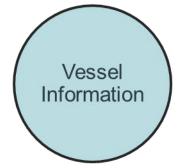
Vessel Wake Prediction Tool



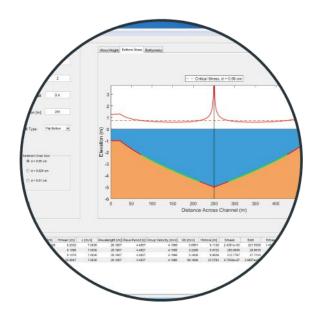
Input



- Flow measurements
- Channel geometry
- Bank characteristics (e.g., mud, sand, oysters)
- Sediment type & distribution



- Speed
- Draft, Beam, Length
- Traffic Density



Output

Wave height distribution, energy flux due to commercial & recreational vessel traffic.



Primary Approach

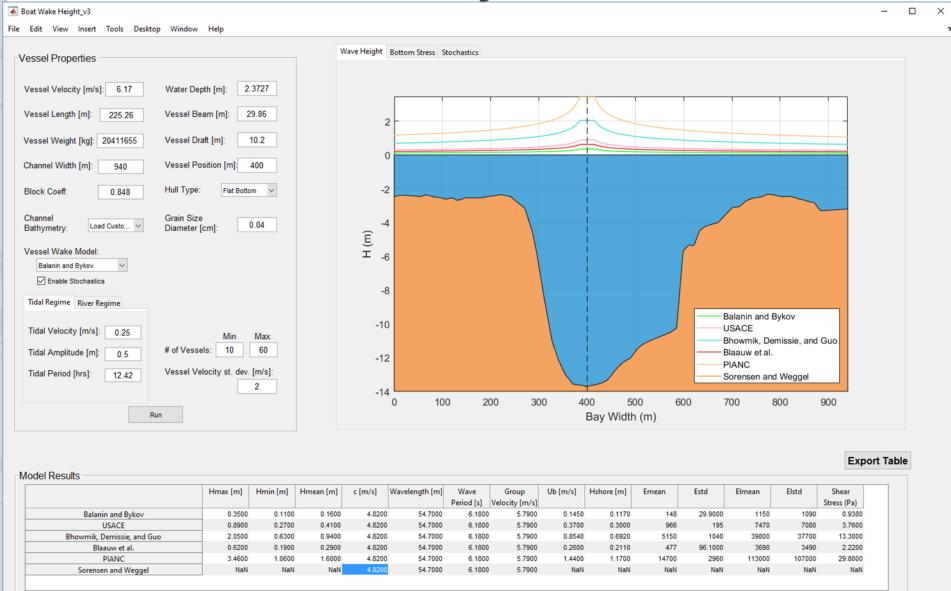


Past Work Summary

- Construct GUI based on available model formulations
- Develop capability to evaluate vessel wake effects given potential change in vessel activity
- Utilize higher fidelity models & data to reduce uncertainty

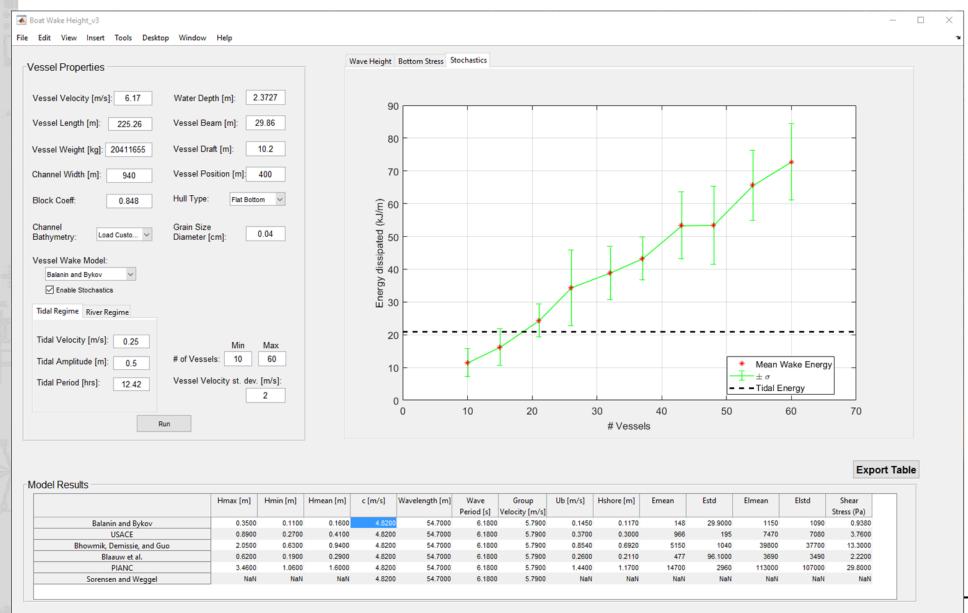


Screen Shot of Primary Interface





Vessel Stochastics





Export Results to Microsoft Excel



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| - Pormat Painter | i – i – <u>–</u> | , , , , , , | ge at came. | ' | , , , , | Formatting Table | | | | | | | - | * * | e Cle | | ilter - Select | 2* |
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| A A | _ | C | D | Е | F | G | Н | 1 | J | K | L | М | N | 0 | P | Q | R | |
| Vessel Velocity [m/s] | | Water Depth [m] | 2.3727 | | | | | | | | | | | | | | | |
| Vessel Length [m] | | Vessel Beam [m] | 29.86 | | | | | | | | | | | | | | | |
| Vessel Weight [kg] | | Vessel Draft [m] | 10.2 | | | | | | | | | | | | | | | |
| Channel Width [m] | | Vessel Position | 400 | | | | | | | | | | | | | | | |
| Block Coeff | | Hull Type | Flat Bottom | | | | | | | | | | | | | | | |
| Channel Bathymetry | C:\Users\rdchlmah\ | Grain Size Diameter [cm] | 0.04 | | | | | | | | | | | | | | | |
| Model Statistics | | | | | | | | | | | | | | | | | | |
| | Hmax [m] | Hmin [m] | Hmean [m] | c [m/s] | Wavelength [m] | Wave Period [s] | Group Velocity [m/s] | Ub [m/s] | Hshore [m | Emean | Estd | Elmean | Elstd | Shear Stre | ss (Pa) | | | |
| Balanin and Bykov | 0.35 | 0.11 | 0.16 | 4.82 | 54.7 | 6.18 | 5.79 | 0.145 | 0.117 | 148 | 29.9 | 1150 | 1090 | 0.938 | | | | |
| USACE | 0.89 | 0.27 | 0.41 | 4.82 | 54.7 | 6.18 | 5.79 | 0.37 | 0.3 | 966 | 195 | 7470 | 7080 | 3.76 | | | | |
| Bhowmik, Demissie, and Guo | 2.05 | 0.63 | 0.94 | 4.82 | 54.7 | 6.18 | 5.79 | 0.854 | 0.692 | 5150 | 1040 | 39800 | 37700 | 13.3 | | | | |
| 3 Blaauw et al. | 0.62 | 0.19 | 0.29 | 4.82 | 54.7 | 6.18 | 5.79 | 0.26 | 0.211 | 477 | 96.1 | 3690 | 3490 | 2.22 | | | | |
| 4 PIANC | 3.46 | 1.06 | 1.6 | 4.82 | 54.7 | 6.18 | 5.79 | 1.44 | 1.17 | 14700 | 2960 | 113000 | 107000 | 29.8 | | | | |
| 5 Sorensen and Weggel | | | | | | | | | | | | | | | | | | |
| 6 | | | | | | | | | | | | | | | | | | |
| 7 Model Wave Heights | | | | | | | | | | | | | | | | | | |
| 8 x (m) | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | |
| 9 Depth (m) | 2.462680749 | 2.462680749 | 2.456719659 | 2.450499 | 2.444277882 | 2.438056932 | 2.431835982 | 2.425615 | 2.419394 | 2.413173 | 2.406952 | 2.400731 | 2.39451 | 2.388289 | 2.382068 | 2.382502 | 2.384078 | 2. |
| Balanin and Bykov | 0.117485723 | 0.11758281 | 0.117680221 | 0.117778 | 0.117876024 | 0.117974419 | 0.118073146 | 0.118172 | 0.118272 | 0.118371 | 0.118471 | 0.118572 | 0.118673 | 0.118774 | 0.118875 | 0.118977 | 0.119079 | 0. |
| 1 USACE | 0.29993381 | 0.300181668 | 0.300430353 | 0.30068 | 0.300930225 | 0.301181423 | 0.301433467 | 0.301686 | 0.30194 | 0.302195 | 0.30245 | 0.302707 | 0.302964 | 0.303222 | 0.303481 | 0.303741 | 0.304002 | 0. |
| Bhowmik, Demissie, and Guo | 0.692322325 | 0.692894442 | 0.69346847 | 0.694044 | 0.694622301 | 0.695202127 | 0.695783908 | 0.696368 | 0.696953 | 0.697541 | 0.698131 | 0.698723 | 0.699316 | 0.699912 | 0.70051 | 0.70111 | 0.701712 | 0. |
| 3 Blaauw et al. | 0.210652812 | 0.21082689 | 0.211001549 | 0.211177 | 0.211352625 | 0.211529049 | 0.211706067 | 0.211884 | 0.212062 | 0.212241 | 0.21242 | 0.2126 | 0.212781 | 0.212962 | 0.213144 | 0.213327 | 0.21351 | 0. |
| 4 PIANC | 1.168719117 | 1.169684916 | | | 1.172601739 | 1.173580551 | 1.174562664 | | | | | 1.179523 | 1.180526 | | | | | |
| 5 Sorensen and Weggel | | | | | | | | | | | | | | | | | | |
| 6 | | | | | | | | | | | | | | | | | | |
| 7 Model Bottom Stress (N/m^2) | Critical Stress = 0.58 | 4 N/m^2 | | | | | | | | | | | | | | | | |
| 8 x (m) | 0 | | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | |
| 9 Depth (m) | 2.462680749 | _ | 2.456719659 | - | 2.444277882 | 2.438056932 | 2.431835982 | | 2.419394 | 2.413173 | | | | | | 2.382502 | | |
| D Balanin and Bykov | 0.938337836 | | | | 0.949044784 | 0.952302936 | 0.955579938 | | | | | 0.972253 | | | 0.982494 | | | |
| 1 USACE | 3.755133537 | | 3.772623078 | | 3.799233067 | 3.812654837 | 3.826155271 | | | | | | | | | | | |
| 2 Bhowmik, Demissie, and Guo | 13.32744175 | | | | 13.4869791 | 13.53554081 | 13.58439005 | | | | | | 13.88366 | | | | 14.01184 | |
| Blaauw et al. | 2.215971589 | | 2.226194366 | | 2.241747492 | 2.249592023 | 2.257482339 | | | | | | | | | 2.324885 | | |
| 4 PIANC | 29.80699803 | | 29.95015091 | | 30.16799253 | 30.27788635 | 30.38843574 | | | | | | | | | 31.33337 | | |
| 5 Sorensen and Weggel | 25.00055005 | 25.0.1303334 | | _0,00070 | 50120153203 | 30.27.03033 | 55,555,74 | 20112200 | -0102202 | - 517 2 107 | 20.0070 | | -2100002 | | -2127.22 | -2100007 | _1,00000 | - |
| Sheet1 + | | | | | | | | | | | | | | | | | | |

Empirical Recreational Vessel Wake Modeling



Maynord (2005) Wave Height from Planing and Semi-planing Small Boats

$$\frac{H_m}{W^{1/3}} = C_m F_w^{-0.58} \left(\frac{x}{W^{1/3}}\right)^{-0.42}$$

Where:

 H_m is predicted wake height

W is displaced volume

x is distance from the vessel centerline

 C_m is the vessel shape coefficient (suggested as 0.82 - 1)

 F_w is the displacement Froude number

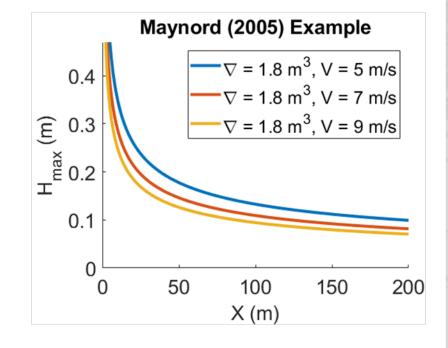
Displacement Froude Number

$$F_w = \frac{V_s}{\sqrt{gW^{1/3}}}$$

Where:

 $V_{\rm s}$ is vessel speed

Note: data forming empirical model is not without substantial scatter



Idealized Numerical Modeling

FUNWAVE

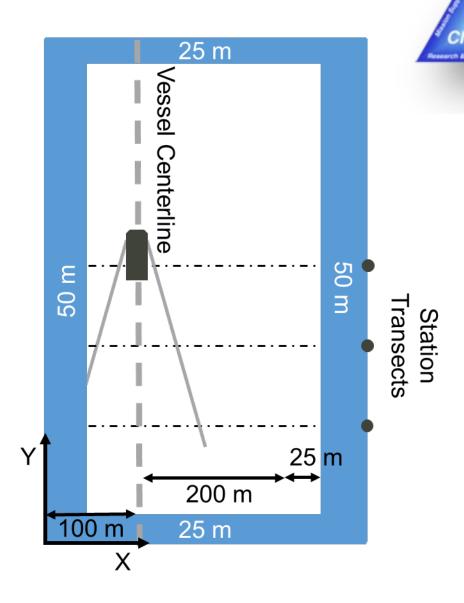
Fully non-linear Boussinesq model (Shi et al. 2012)

https://fengyanshi.github.io/build/html/index.html

- Includes a ship-wake module
 - Validated against laboratory experiments (Gorlay, 2001) in Shi et al. (2018)

Idealized Simulations

- Simulating a single vessel, traveling through a flat domain
- Domain Size: 375 m x 1,110 m 1,925 m
- Depth (Constant): 1.75 m
- Detailed output:
 - Stations along 3 transects





Intended Vessel Wake Numerical Modeling Regime



Intended Model Regime

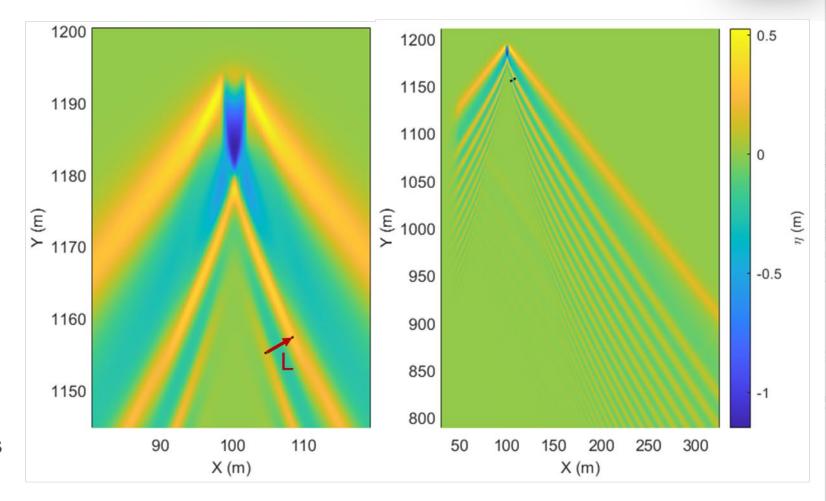
Intermediate and shallow water waves

$$k \cdot h < \pi$$

$$h < \frac{L}{2}$$

Simulated Wake Length

- Wake length estimated as the distance between peaks near the vessel
- Manual point selection (accuracy with 0.2 m cells)
- Issues encountered in simulations with L/2 < h

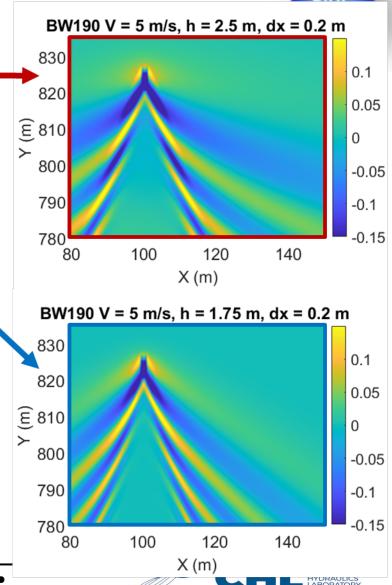


Test Simulations Relative to Intended Wake Regime



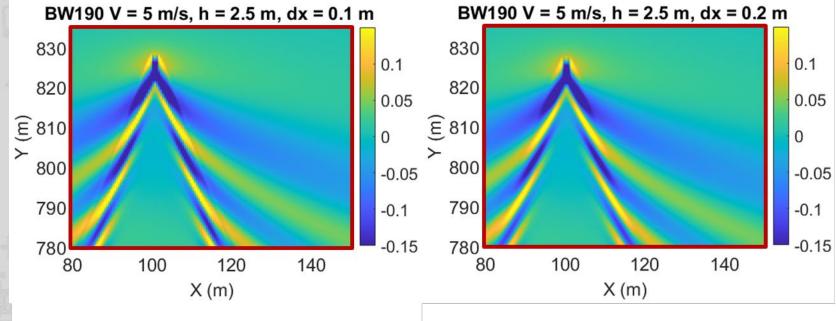
| Vessel | Speed | Depth | Wake Length | kh/π |
|--------|-------|--------|-------------|-----------|
| BW190 | 5 m/s | 2.5 m | 3.5 – 4.5 m | 1.1 – 1.4 |
| BW190 | 5 m/s | 1.75 m | 3.5 – 4.5 m | 0.8 – 1 |
| BW190 | 7 m/s | 3.5 m | 3.5 – 4.5 m | 1.6 – 2 |
| BW190 | 7 m/s | 1.75 m | 3.5 – 4.5 m | 0.8 – 1 |

- Manual selection accuracy estimated as ~ ± 2 cells
- Changes in minimum wake length are less than method accuracy
- No noticeable wake length changes with tested depths
 & speeds
- Minimum wake lengths are sometimes greater than minima for intended regime (kh<π)
- Maynord (2005) model appears to be from scenarios in which kh > π for the minimum wake length (h > 3.5 m).



Wake Length and Depth Impact (2 Ton Vessel, 5 m/s)

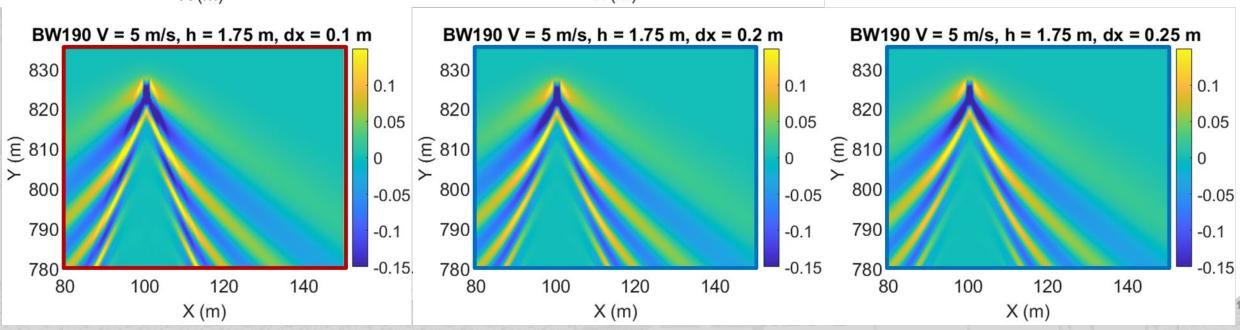




Results

Differences noticed between

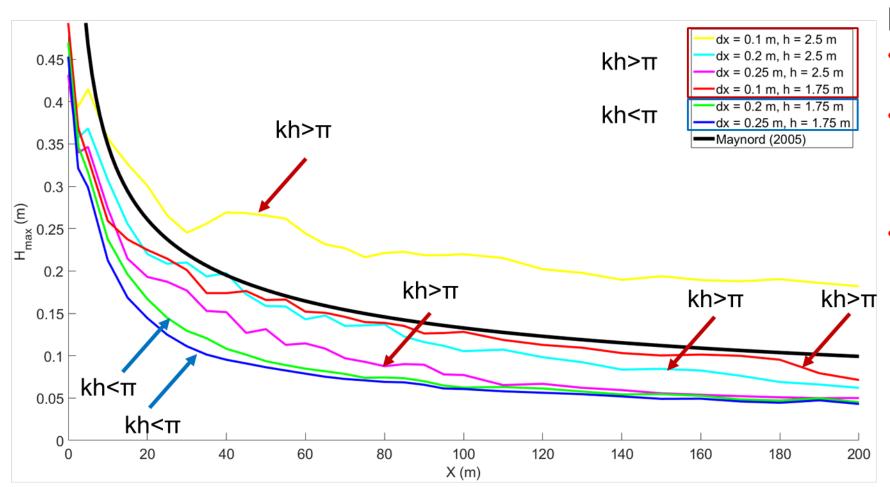
$$kh < \pi$$



Idealized Numerical Model Solutions (Depth and Resolution Impact)



2 Ton Vessel, 5 m/s



Results

- H_{max} vary substantially where kh > π
- Results where kh < π
 appear to be reasonable,
 but H_{max} in these scenarios
 may be limited by depth.
- Concerns on adequately resolving wakes remain



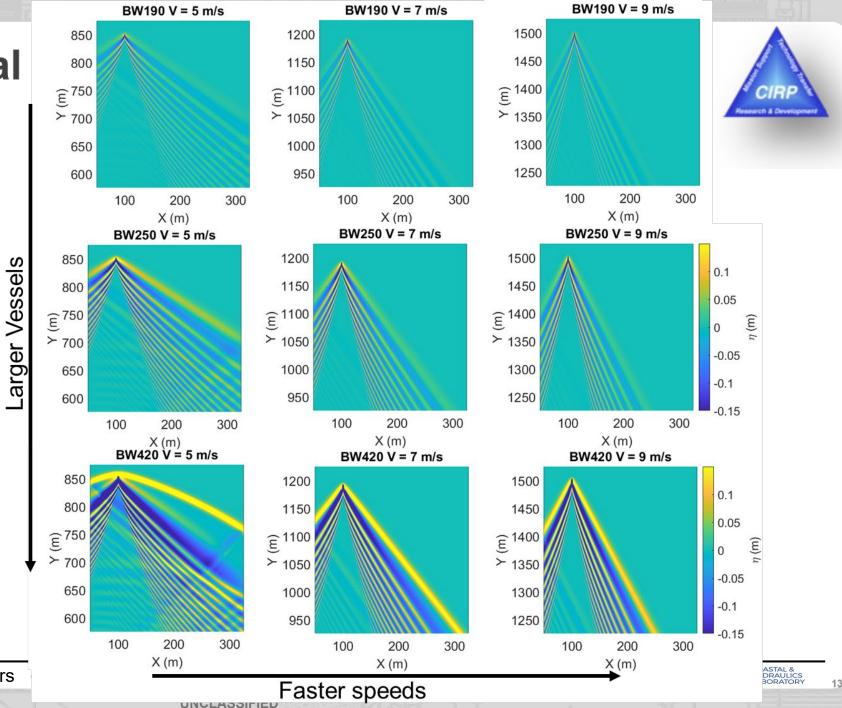
Idealized Numerical Model Test Matrix

Vessel

- BW190: 2 Ton
- BW250: 6 Ton
- BW420: 23 Ton

Speed

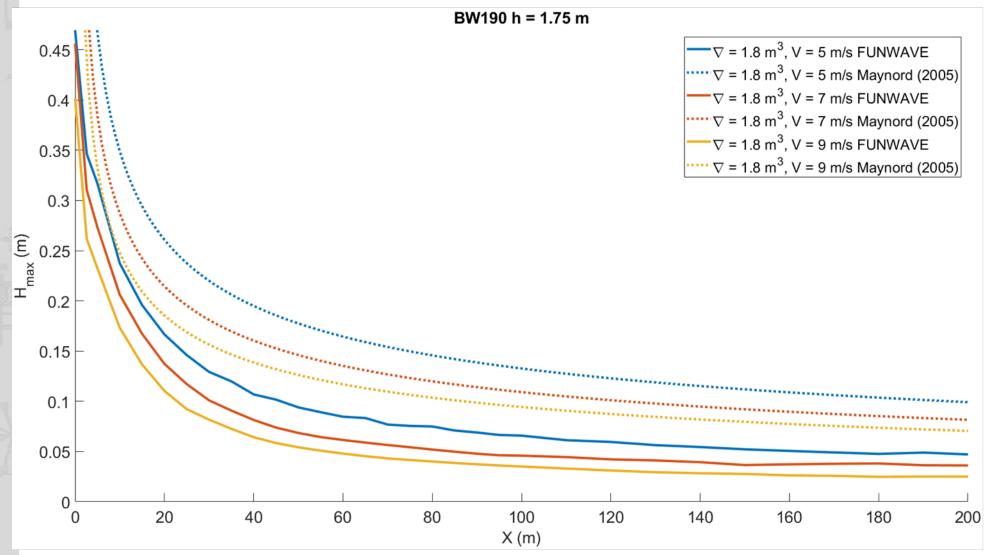
- Completed: 5 m/s (10 knots), 7 m/s (14 knots), 9 m/s (18 knots)
- Larger vessels cause substantial reflection.
 - Particularly at slower speeds
 - Testing underway to reduce reflections



Empirical vs. Idealized Numerical Model Solutions

2 Ton Vessel





Results

- H_{max} decreases
 with vessel speed
 and distance,
 following findings
 of Maynord (2005)
- $H_{max} \sim \frac{1}{2}$ of Maynord (2005) prediciton
- Maynord (2005) data collected in > 3.5 m depth
 - Depth limited solution?

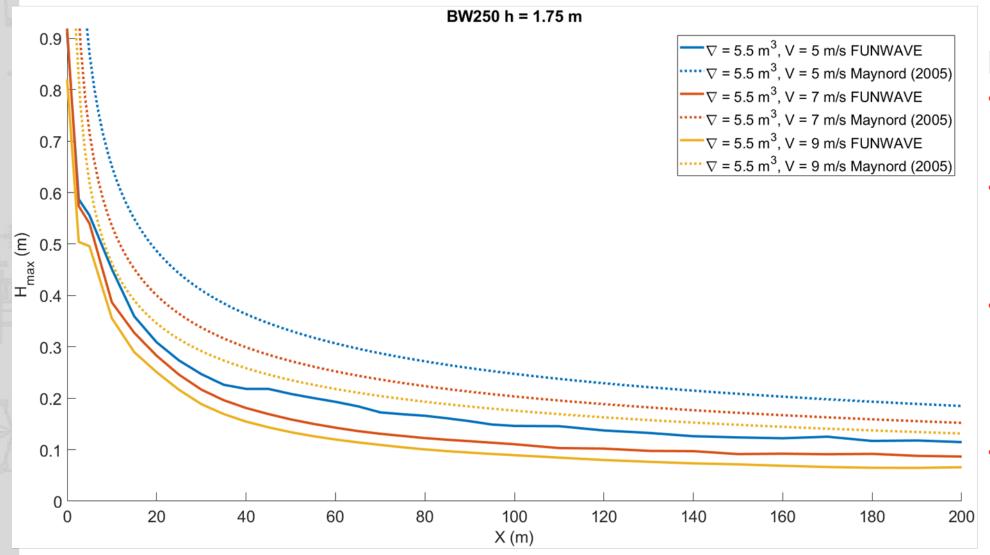
US Army Corps of Engineers • Engineer Research and Development Center •



Empirical vs. Idealized Numerical Model Solutions

6 Ton Vessel





Results

- H_{max} decreases
 with vessel speed
 and distance.
- Less substantial
 H_{max} decrease
 with velocity than
 2 ton vessel
- Maynord (2005)
 model developed
 with vessels
 lighter than 1.6
 tons
- Reflection likely impacts results.
 Working on less reflective domains.

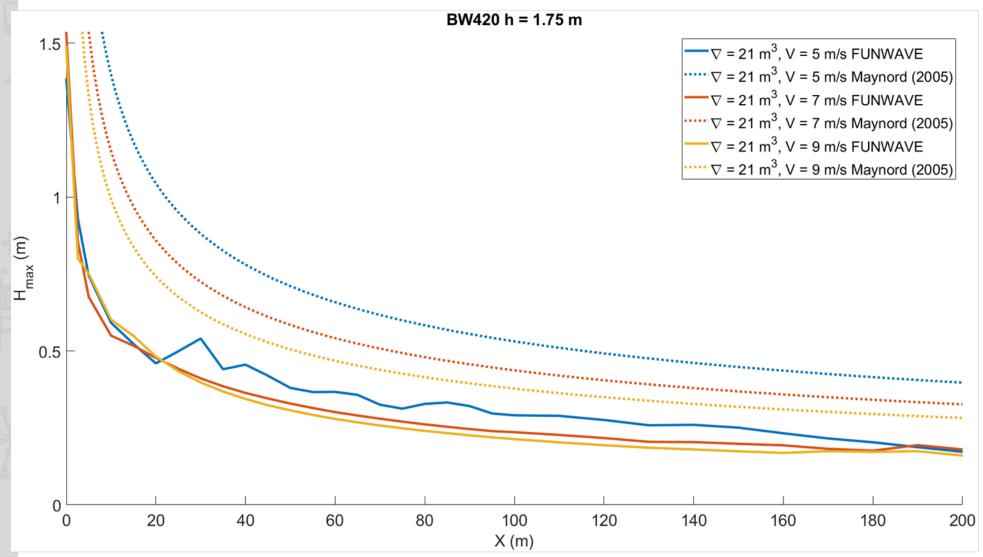
US Army Corps of Engineers • Engineer Research and Development Center •



Empirical vs. Idealized Numerical Model Solutions

23 Ton Vessel





Results

- H_{max} does not decrease with speed
- Reflection likely impacts results.
 Working on less reflective domains.
- Maynord (2005)
 model developed
 with vessels
 lighter than 1.6
 tons



Summary

Reasonable Recreational Vessel Wake Results



Approaching reasonable solutions for relatively large recreational vessels in relatively shallow water

Persistent Issues

- Depth impact on solutions and the ability to assess the upper limit of vessel wake forcing
- Resolution dependence

Conclusions

Applicability for Scoping Level Recreational Vessel Wake Estimates

- Reliable solution matrix for a wide variety of conditions?
- Possibility remains for improved estimates of wake characteristics directly impacting edge erosion





Thank You! Questions?

